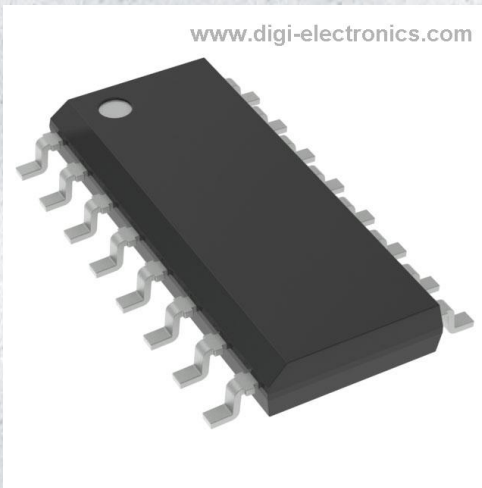


# VIPER38LDTR Datasheet



<https://www.DiGi-Electronics.com>

DiGi Electronics Part Number	VIPER38LDTR-DG
Manufacturer	<a href="#">STMicroelectronics</a>
Manufacturer Product Number	VIPER38LDTR
Description	IC OFFLINE SWITCH FLYBACK 16SO
Detailed Description	Converter Offline Flyback Topology 60kHz 16-SO

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## Purchase and inquiry

Manufacturer Product Number:

VIPER38LDTR

Series:

VIPer™ plus

Output Isolation:

Isolated

Voltage - Breakdown:

800V

Voltage - Start Up:

14 V

Duty Cycle:

80%

Power (Watts):

20 W

Control Features:

-

Package / Case:

16-SOIC (0.154", 3.90mm Width)

Mounting Type:

Surface Mount

Manufacturer:

STMicroelectronics

Product Status:

Active

Internal Switch(s):

Yes

Topology:

Flyback

Voltage - Supply (Vcc/Vdd):

8.5V ~ 23.5V

Frequency - Switching:

60kHz

Fault Protection:

Current Limiting, Over Temperature, Over Voltage, Short Circuit

Operating Temperature:

-40°C ~ 150°C (TJ)

Supplier Device Package:

16-SO

Base Product Number:

VIPER38

## Environmental & Export classification

RoHS Status:

ROHS3 Compliant

REACH Status:

REACH Unaffected

HTSUS:

8542.39.0001

Moisture Sensitivity Level (MSL):

3 (168 Hours)

ECCN:

EAR99

## VIPerPlus family: peak power high-voltage converter

Datasheet - production data

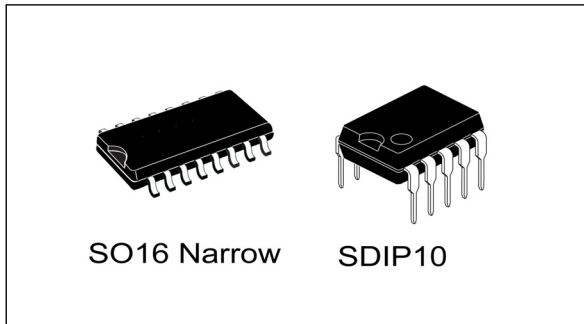
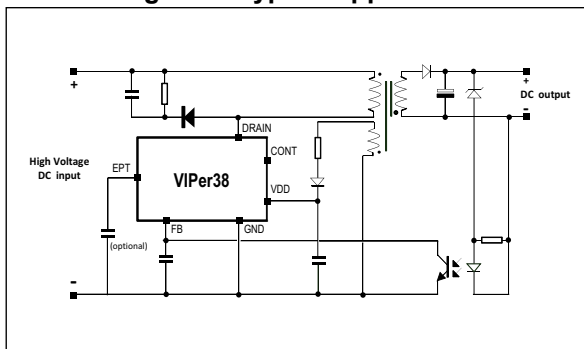


Figure 1. Typical application



## Features

- 800 V avalanche-rugged power MOSFET allowing ultra wide range input  $V_{ac}$  to be achieved
- Embedded HV start-up and sense FET
- PWM current-mode controller
- OCP with selectable threshold ( $I_{Dlim}$ ) and 2<sup>nd</sup> OCP with higher value ( $I_{DMAX}$ ) to protect the IC from transformer saturation or short-circuit of the secondary diode
- 30 mW no-load consumption at 230 V<sub>ac</sub>
- Two operating frequencies:
  - 60 kHz (L type) or 115 kHz (H type)
- Jittered frequency reduces the EMI
- Extra power timer (EPT) blanks the overload current for few seconds

- Output overvoltage protection with tight tolerance and digital noise filter
- Soft-start reduces the stress during startup and increases IC lifetime
- Automatic restart after a fault condition
- Thermal shutdown increases system reliability and IC lifetime

## Applications

- Auxiliary power supply for consumer and home equipment
- Power supply for energy meters and data concentrators
- Adapters

## Description

The device is a high-voltage converter that smartly integrates an 800 V rugged power MOSFET with PWM current-mode control. The power MOSFET allows a very high input  $V_{ac}$  to be applied, just limited from its breakdown voltage. This IC is capable of meeting more stringent energy-saving standards as it has very low consumption and operates in burst mode under light load.

The device features an adjustable extra power timer (EPT) that enables the IC to sustain overload conditions for a few seconds.

The integrated HV startup, sense FET and oscillator with jitter allow the advantage of using minimal components in the application.

The device features high-level protections like dual-level OCP, output overvoltage, short-circuit, and thermal shutdown with hysteresis. After the removal of a fault condition, the IC is automatically restarted.

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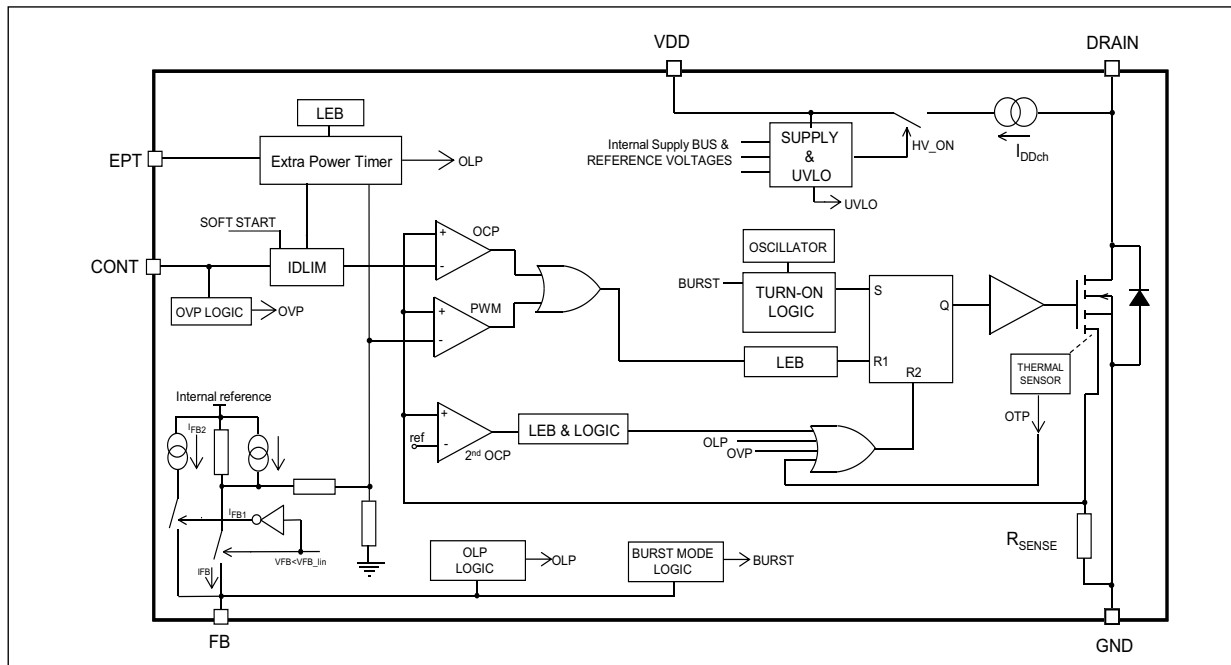
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## 1 Block diagram

Figure 2. Block diagram



## 2 Typical power

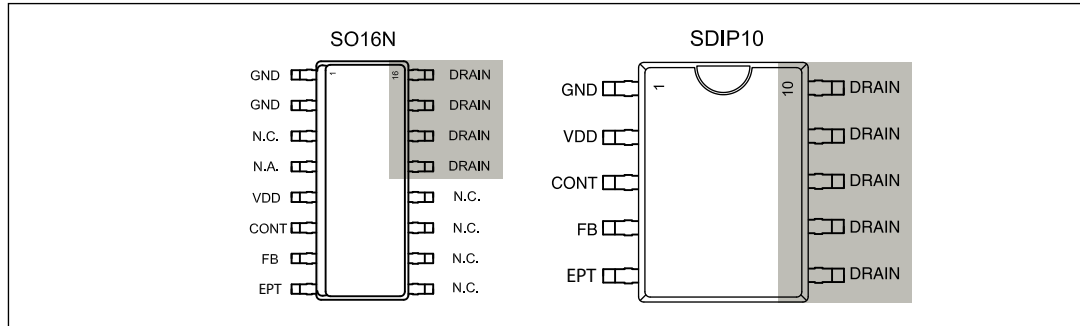
Table 1. Typical power

Nominal power	230 V <sub>AC</sub>		85-265 V <sub>AC</sub>	
	Adapter <sup>(1)</sup>	Open frame <sup>(2)</sup>	Adapter <sup>(1)</sup>	Open frame <sup>(2)</sup>
VIPER38	18 W	20 W	13 W	15 W
	28 W (peak) <sup>(3)</sup>	30 W (peak) <sup>(3)</sup>	23 W (peak) <sup>(3)</sup>	25 W (peak) <sup>(3)</sup>

1. Typical continuous power in non-ventilated enclosed adapter measured at 50 °C ambient.
2. Maximum practical continuous power in an open frame design at 50 °C ambient, with adequate heat sinking.
3. Maximum practical peak power at 50 °C ambient, with adequate heat sinking for 2 sec (max).

### 3 Pin settings

Figure 3. Connection diagram (top view)



Note: The copper area for heat dissipation has to be designed under the DRAIN pins.

Table 2. Pin description

SO16N	Name	Function
1, 2	GND	Device ground and source of the power MOSFET.
3	N.C.	Not connected.
4	N.A.	Not available for user. This pin is mechanically connected to the controller die pad of the frame. In order to improve the noise immunity, is highly recommended connect it to GND (pin 1-2).
5	VDD	Supply voltage of the control section. This pin also provides the charging current of the external capacitor during startup.
6	CONT	Control pin. The following functions can be selected: 1. current limit setpoint adjustment. The default value (set internally) of the cycle-by-cycle current limit can be reduced by connecting an external resistor to ground. 2. output voltage monitoring. A voltage exceeding the $V_{OVP}$ threshold (see <a href="#">Table 8: Controller section on page 9</a> ) shuts the IC down, reducing device consumption. This function is strobed and digitally filtered for high noise immunity.
7	FB	Control input for duty cycle control. The internal current generator provides bias current for loop regulation. A voltage below the threshold $V_{FBbm}$ activates burst-mode operation. A level close to the threshold $V_{FBlin}$ means that we are approaching the cycle-by-cycle overcurrent setpoint.
8	EPT	This pin allows the connection of an external capacitor for extra power management. If the function is not used, the pin has to be connected to GND.
9...12	N.C.	Not connected.
13...16	DRAIN	High-voltage drain pin. The built-in high-voltage switched startup bias current is drawn from this pin too. These pins are connected to the metal frame to facilitate heat dissipation.

## 4 Electrical characteristics

**Table 3. Absolute maximum ratings**

Symbol	Parameter	Value		Unit
		Min	Max	
V <sub>DRAIN</sub>	Drain-to-source (ground) voltage		800	V
I <sub>DRAIN</sub>	Pulse drain current (limited by T <sub>J</sub> = 150 °C)		3	A
V <sub>CONT</sub>	Control input pin voltage	-0.3	6	V
V <sub>FB</sub>	Feedback voltage	-0.3	5.5	V
V <sub>EPT</sub>	EPT input pin voltage	-0.3	5	V
V <sub>DD</sub>	Supply voltage (I <sub>DD</sub> = 25 mA)	-0.3	Self limited	V
I <sub>DD</sub>	Input current		25	mA
P <sub>TOT</sub>	Power dissipation at T <sub>A</sub> < 60 °C		1.5	W
T <sub>J</sub>	Operating junction temperature range	-40	150	°C
T <sub>STG</sub>	Storage temperature	-55	150	°C

**Table 4. Thermal data**

Symbol	Parameter	Max		Unit
		SDIP10	SO16N	
R <sub>TH-JC</sub>	Thermal resistance junction to case <sup>(1)</sup> (Dissipated power = 1 W)	5	10	°C/W
R <sub>TH-JA</sub>	Thermal resistance junction ambient <sup>(1)</sup> (Dissipated power = 1 W)	105	120	°C/W
R <sub>TH-JC</sub>	Thermal resistance junction to case <sup>(2)</sup> (Dissipated power = 1 W)	5	5	°C/W
R <sub>TH-JA</sub>	Thermal resistance junction ambient <sup>(2)</sup> (Dissipated power = 1 W)	90	85	°C/W

1. When mounted on a standard, single side FR4 board with minimum copper area.
2. When mounted on a standard, single side FR4 board with 100 mm<sup>2</sup> of Cu (35 µm thick).

**Table 5. Avalanche ratings**

Symbol	Parameter	Test condition	Value	Unit
I <sub>AS</sub>	Avalanche current	Repetitive or non repetitive (pulse width limited by T <sub>Jmax</sub> )	1.15	A
E <sub>AS</sub>	Single pulse avalanche energy <sup>(1)</sup>	I <sub>D</sub> = I <sub>AS</sub> , V <sub>DS</sub> = 100 V starting T <sub>J</sub> = 25 °C	5	mJ

1. Specification assured by design and characterization.

## Electrical characteristics

## VIPER38

$T_J = -25$  to  $125$  °C,  $V_{DD} = 14$  V; unless otherwise specified (adjust  $V_{DD}$  above  $V_{DDon}$  startup threshold before setting to 14 V).

Table 6. Power section

Symbol	Parameter	Test condition	Min	Typ	Max	Unit
$V_{BVDSS}$	Breakdown voltage	$I_{DRAIN} = 1$ mA, $V_{FB} = GND$ , $T_J = 25$ °C	800			V
$I_{OFF}$	OFF-state drain current	$V_{DRAIN} = \text{max rating}$ , $V_{FB} = GND$ , $T_J = 25$ °C			60	$\mu$ A
$R_{DS(on)}$	Drain-source on-state resistance	$I_{DRAIN} = 0.4$ A, $V_{FB} = 3$ V, $V_{EPT} = GND$ , $T_J = 25$ °C			4.5	$\Omega$
		$I_{DRAIN} = 0.4$ A, $V_{FB} = 3$ V, $V_{EPT} = GND$ , $T_J = 125$ °C			9	$\Omega$
$C_{OSS}$	Effective (energy related) output capacitance	$V_{DRAIN} = 0$ to 640 V, $T_J = 25$ °C		17		pF

Table 7. Supply section

Symbol	Parameter	Test condition	Min	Typ	Max	Unit
<b>Voltage</b>						
$V_{DRAIN\_START}$	Drain-source start voltage		60	80	100	V
$I_{DDch1}$	Startup charging current	$V_{DRAIN} = 120$ V, $V_{EPT} = GND$ , $V_{FB} = GND$ , $V_{DD} = 4$ V	-2	-3	-4	mA
$I_{DDch2}$	Restart charging current (after fault)	$V_{DRAIN} = 120$ V, $V_{EPT} = GND$ , $V_{FB} = GND$ , $V_{DD} = 4$ V	-0.4	-0.6	-0.8	mA
$V_{DD}$	Operating voltage range	After turn-on	8.5		23.5	V
$V_{DDclamp}$	$V_{DD}$ clamp voltage	$I_{DD} = 20$ mA	23.5			V
$V_{DDon}$	$V_{DD}$ startup threshold	$V_{DRAIN} = 120$ V, $V_{EPT} = GND$ , $V_{FB} = GND$	13	14	15	V
$V_{DDoff}$	$V_{DD}$ undervoltage shutdown threshold		7.5	8	8.5	V
$V_{DD(RESTART)}$	$V_{DD}$ restart voltage threshold	$V_{DRAIN} = 120$ V, $V_{EPT} = GND$ , $V_{FB} = GND$	4	4.5	5	V
<b>Current</b>						
$I_{DD0}$	Operating supply current, not switching	$V_{FB} = GND$ , $F_{OSC} = 0$ kHz $V_{EPT} = GND$ , $V_{DD} = 10$ V			0.7	mA
$I_{DD1}$	Operating supply current, switching	$V_{DRAIN} = 120$ V, $F_{OSC} = 60$ kHz			2.5	mA
		$V_{DRAIN} = 120$ V, $F_{OSC} = 115$ kHz			3.5	mA
$I_{DD\_FAULT}$	Operating supply current, with protection tripping	$V_{DD} = 10$ V			400	$\mu$ A
$I_{DD\_OFF}$	Operating supply current with $V_{DD} < V_{DD\_OFF}$	$V_{DD} = 7$ V			270	$\mu$ A

Table 8. Controller section

Symbol	Parameter	Test condition	Min	Typ	Max	Unit
<b>Feed-back pin</b>						
$V_{FBolp}$	Overload shutdown threshold		4.5	4.8	5.2	V
$V_{FBlin}$	Overload detection threshold		3.2	3.5	3.7	V
$V_{FBbm}$	Burst mode threshold	Voltage falling	0.54	0.6	0.66	V
$V_{FBbmhys}$	Burst mode hysteresis	Voltage rising		90		mV
$I_{FB1}$	Feedback sourced current	$V_{FB} = 0.3\text{ V}$	-150	-200	-280	uA
$I_{FB2}$	Feedback current-OLP delay	$V_{FBlin} < V_{FB} < V_{FBolp}$		-3		uA
$R_{FB(DYN)}$	Dynamic resistance	$V_{FB} < 3.3\text{ V}$	14		21	k $\Omega$
$H_{FB}$	$\Delta V_{FB} / \Delta I_D$		0.5		2	V/A
<b>CONT pin</b>						
$V_{CONT\_l}$	Low-level clamp voltage	$I_{CONT} = -100\ \mu\text{A}$	0.4	0.5	0.6	V
$V_{CONT\_h}$	High-level clamp voltage	$I_{CONT} = 1\text{ mA}$	5	5.5	6	V
<b>Current limitation</b>						
$I_{Dlim}$	Max drain current limitation	$V_{FB} = 4\text{ V}$ , $I_{CONT} = -10\ \mu\text{A}$ $T_J = 25\text{ }^\circ\text{C}$	1.07	1.15	1.23	A
$t_{SS}$	Soft-start time		7.6	8.5	9.4	ms
$t_{ON\_MIN}$	Minimum turn-on time		220	400	480	ns
$t_d$	Propagation delay	(1)		20		ns
$t_{LEB}$	Leading edge blanking	(1)		380		ns
$I_{D\_BM}$	Peak drain current during burst mode	$V_{FB} = 0.6\text{ V}$	115	190	265	mA
<b>Oscillator section</b>						
$F_{OSC}$	$V_{FB} = 1\text{ V}$	VIPER38L	54	60	66	kHz
		VIPER38H	103	115	127	kHz
FD	Modulation depth	VIPER38L		$\pm 4$		kHz
		VIPER38H		$\pm 8$		kHz
FM	Modulation frequency		830	920	1010	Hz
$D_{MAX}$	Maximum duty cycle		70		80	%
<b>Overcurrent protection (2<sup>nd</sup> OCP)</b>						
$I_{DMAX}$	Second overcurrent threshold			1.7		A
<b>Overvoltage protection</b>						
$V_{OVP}$	Overvoltage protection threshold		2.7	3	3.3	V
$t_{STROBE}$	Overvoltage protection strobe time		1.5	2	2.5	$\mu\text{s}$

## Electrical characteristics

## VIPER38

Table 8. Controller section (continued)

Symbol	Parameter	Test condition	Min	Typ	Max	Unit
<b>Extra power management</b>						
$I_{DLIM\_EPT}$	Drain current limit with EPT function	(1)		85% $I_{Dim}$		A
$V_{EPT(STOP)}$	EPT shutdown threshold	$I_{CONT} < -10 \mu A$	3.6	4	4.4	V
$V_{EPT(RESTART)}$	EPT restart threshold		0.4	0.6	0.8	V
$I_{EPT}$	Sink/source current		4	5	6	$\mu A$
<b>Thermal shutdown</b>						
$T_{SD}$	Thermal shutdown temperature	(1)	150	160		$^{\circ}C$
$T_{HYST}$	Thermal shutdown hysteresis	(1)		30		$^{\circ}C$

1. Specification assured by design, characterization and statistical correlation.

Figure 4. Minimum turn-on time test circuit

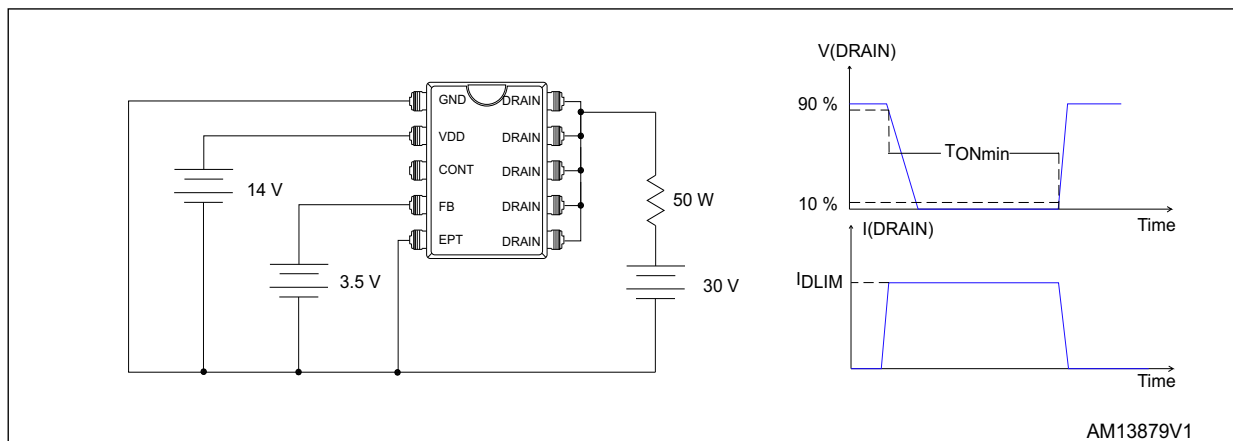
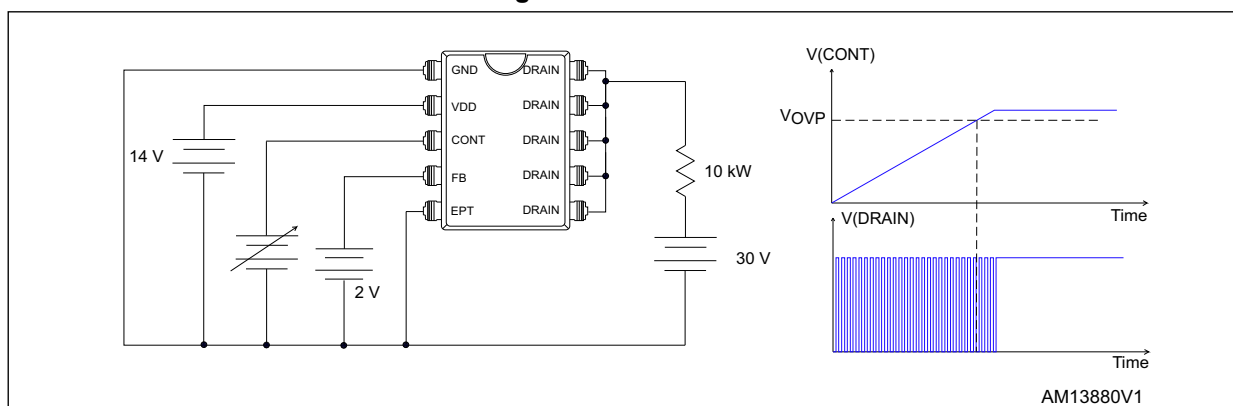
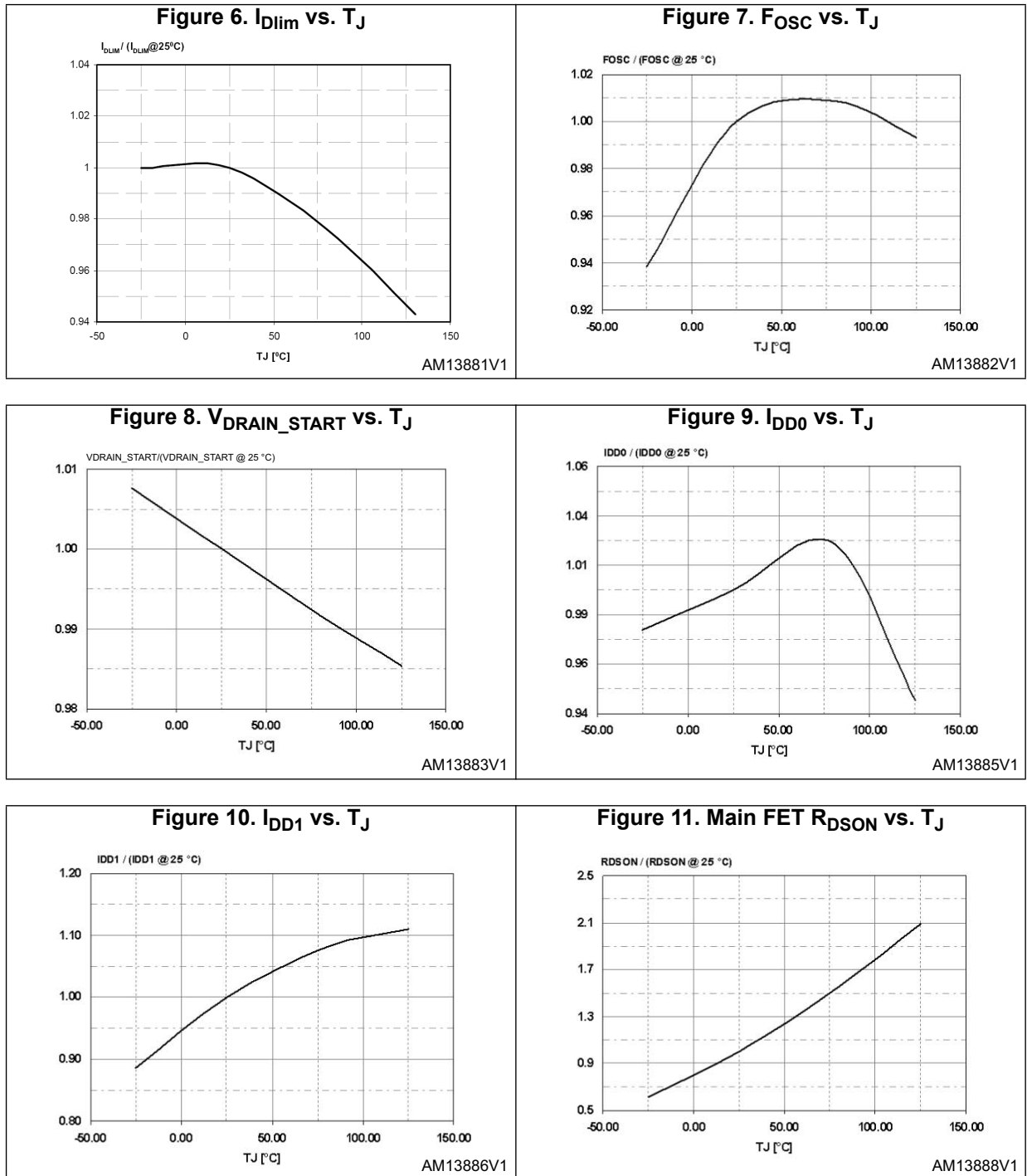


Figure 5. OVP threshold test circuit



Note: Adjust VDD above VDDon startup threshold before setting to 14 V.

## 5 Typical electrical characteristics



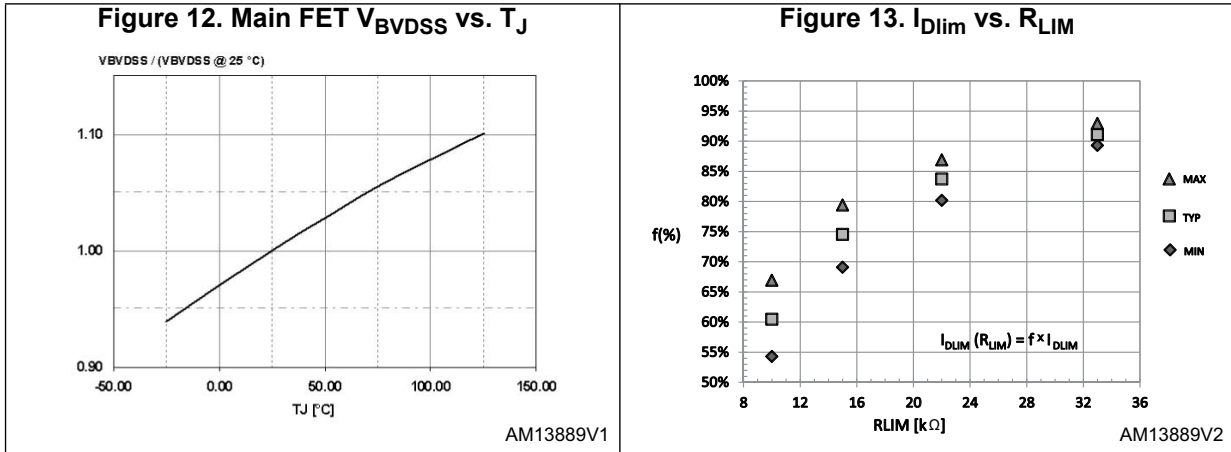
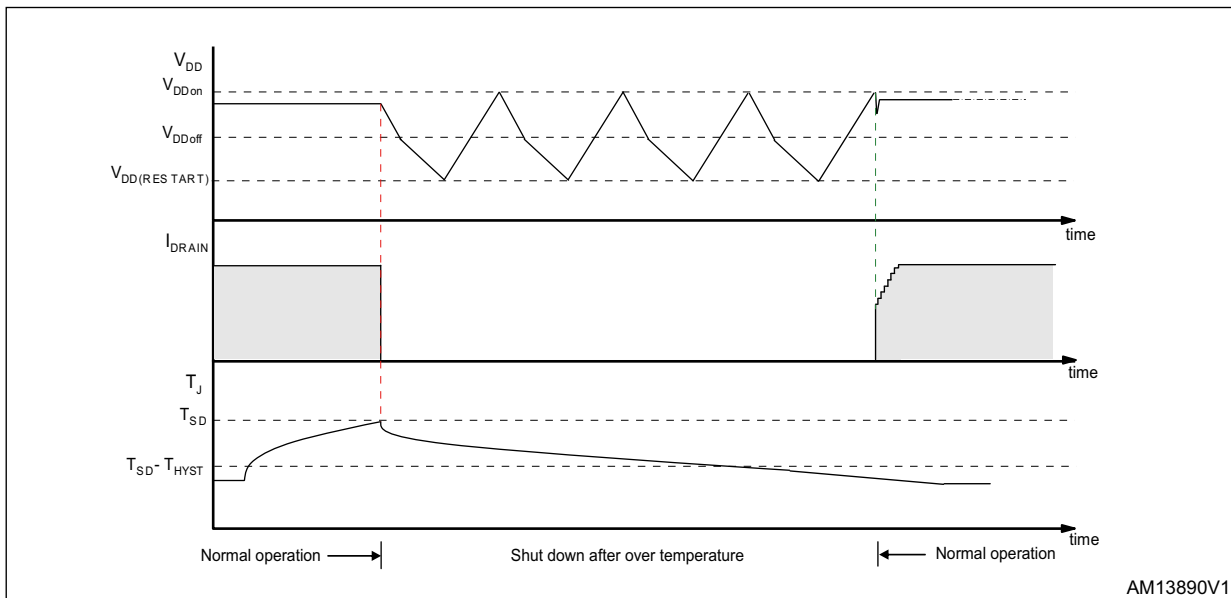


Figure 14. Thermal shutdown



## 6 Typical circuit

Figure 15. Basic flyback application

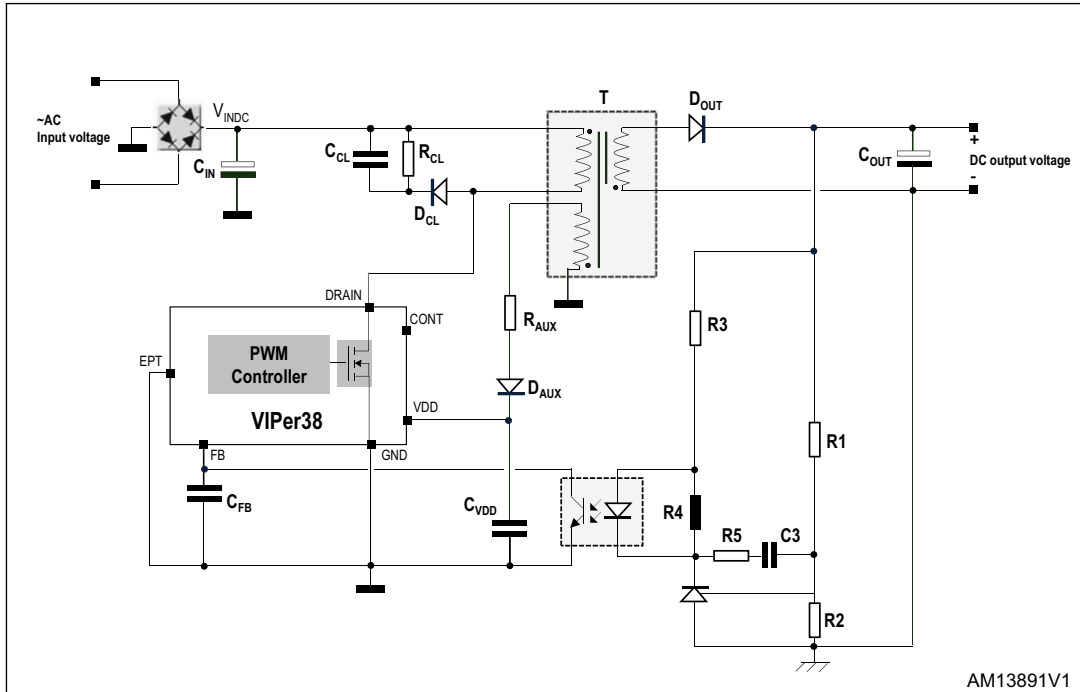
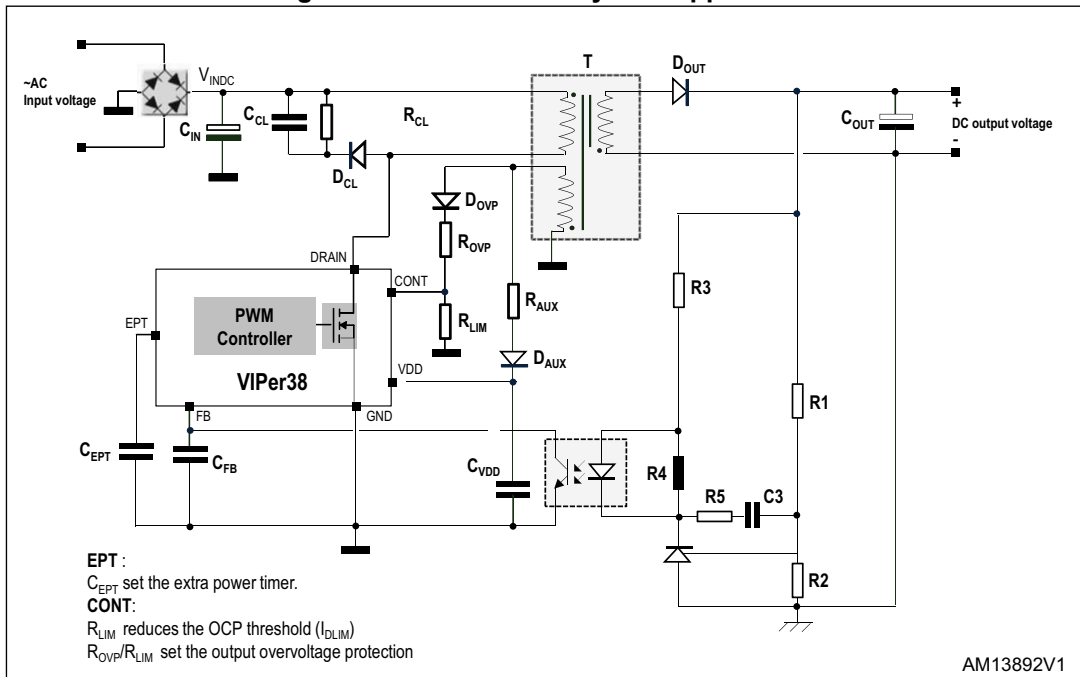


Figure 16. Full-featured flyback application



## 7 Operation

The device is a high-performance low-voltage PWM controller chip with an 800 V, avalanche rugged power section.

The controller includes the oscillator with jitter, startup circuit with soft-start, PWM logic, current limiting circuit with adjustable setpoint, second overcurrent circuit, burst mode management, extra power timer circuit, UVLO circuit, auto-restart circuit and thermal protection circuit.

The current limit setpoint is set by the CONT pin. Burst mode operation guarantees high performance in standby mode and contributes to meeting energy-saving standards.

All the fault protections are built in auto-restart mode with very low repetition rate to prevent the IC from overheating.

### 7.1 Power section and gate driver

The power section is implemented with an avalanche-rugged N-channel MOSFET, which guarantees safe operation within the specified energy rating as well as high dv/dt capability. The power section has a  $B_{VDSS}$  of 800 V min. and a typical  $R_{DS(on)}$  of 4.5  $\Omega$  at 25 °C.

The integrated SenseFET structure allows a virtually loss-less current sensing.

The gate driver is designed to supply a controlled gate current during both turn-on and turn-off in order to minimize common-mode EMI. Under UVLO conditions an internal pull-down circuit holds the gate low in order to ensure that the power section cannot be turned on accidentally.

### 7.2 High-voltage startup generator

The HV current generator is supplied through the DRAIN pin and it is enabled only if the input bulk capacitor voltage is higher than the  $V_{DRAIN\_START}$  threshold, 80 V DC typically. When the HV current generator is ON, the  $I_{DDch1}$  current (3 mA typical value) is delivered to the capacitor on the  $V_{DD}$  pin. During auto-restart mode after a fault event, the current is reduced to  $I_{DDch2}$  (0.6 mA, typ) in order to have a slow duty cycle during the restart phase.

### 7.3 Power-up and soft startup

When the input voltage rises to the device start threshold,  $V_{DRAIN\_START}$ , the  $V_{DD}$  voltage begins to grow due to the  $I_{DDch1}$  current (see [Table 7: Supply section](#)) coming from the internal high-voltage startup circuit. If the  $V_{DD}$  voltage reaches the  $V_{DDon}$  threshold, the power MOSFET starts switching and the HV current generator is turned OFF.

The IC is powered by the energy stored in the capacitor on the  $V_{DD}$  pin,  $C_{VDD}$ , until the self-supply circuit (typically an auxiliary winding of the transformer and a steering diode) develops a voltage high enough to sustain the operation.

The  $C_{VDD}$  capacitor must be correctly sized to avoid fast discharge and keep the required voltage higher than the  $V_{DDoff}$  threshold. In fact, an insufficient capacitance value could terminate the switching operation before the controller receives any energy from the auxiliary winding.

The following formula can be used for the  $C_{VDD}$  capacitor calculation:

### Equation 1

$$C_{VDD} = \frac{I_{DDch1} \times t_{SSaux}}{V_{DDon} - V_{DDoff}}$$

The parameter  $t_{SSaux}$  is the time needed for the steady state of the auxiliary voltage. This time represents an estimate of the user's application according to the output stage configurations (transformer, output capacitances, etc.).

During the converter startup time, the drain current limitation is progressively increased to the maximum value. In this way the stress on the secondary diode is considerably reduced. It also helps to prevent transformer saturation. The soft-start time lasts 8.5 ms and the feature is implemented for every attempt of the startup converter or after a fault.

**Figure 17.  $I_{DD}$  current during startup and burst mode**

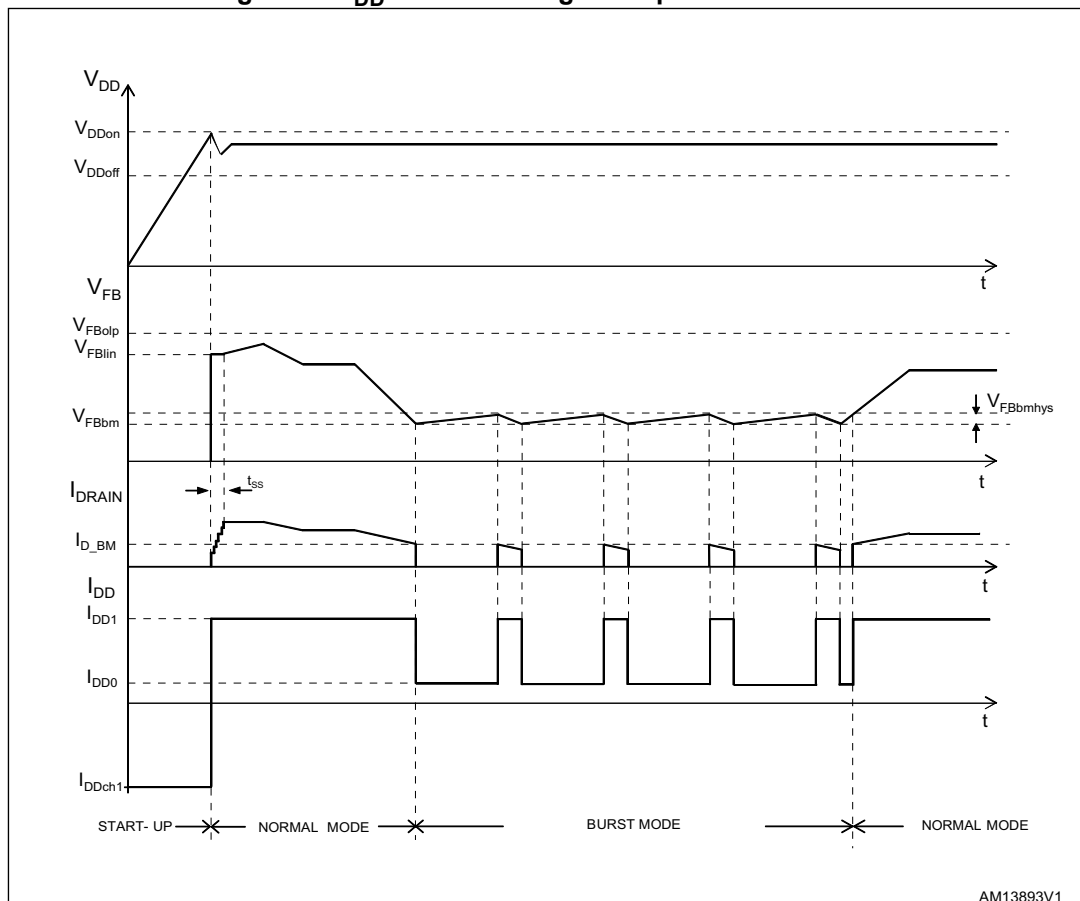


Figure 18. Timing diagram: normal power-up and power-down sequences

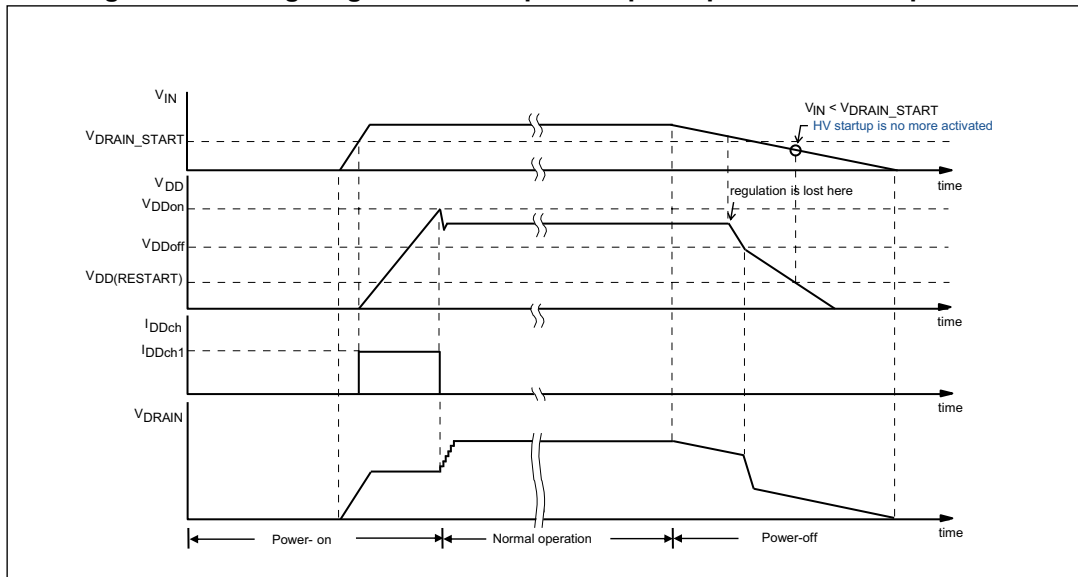
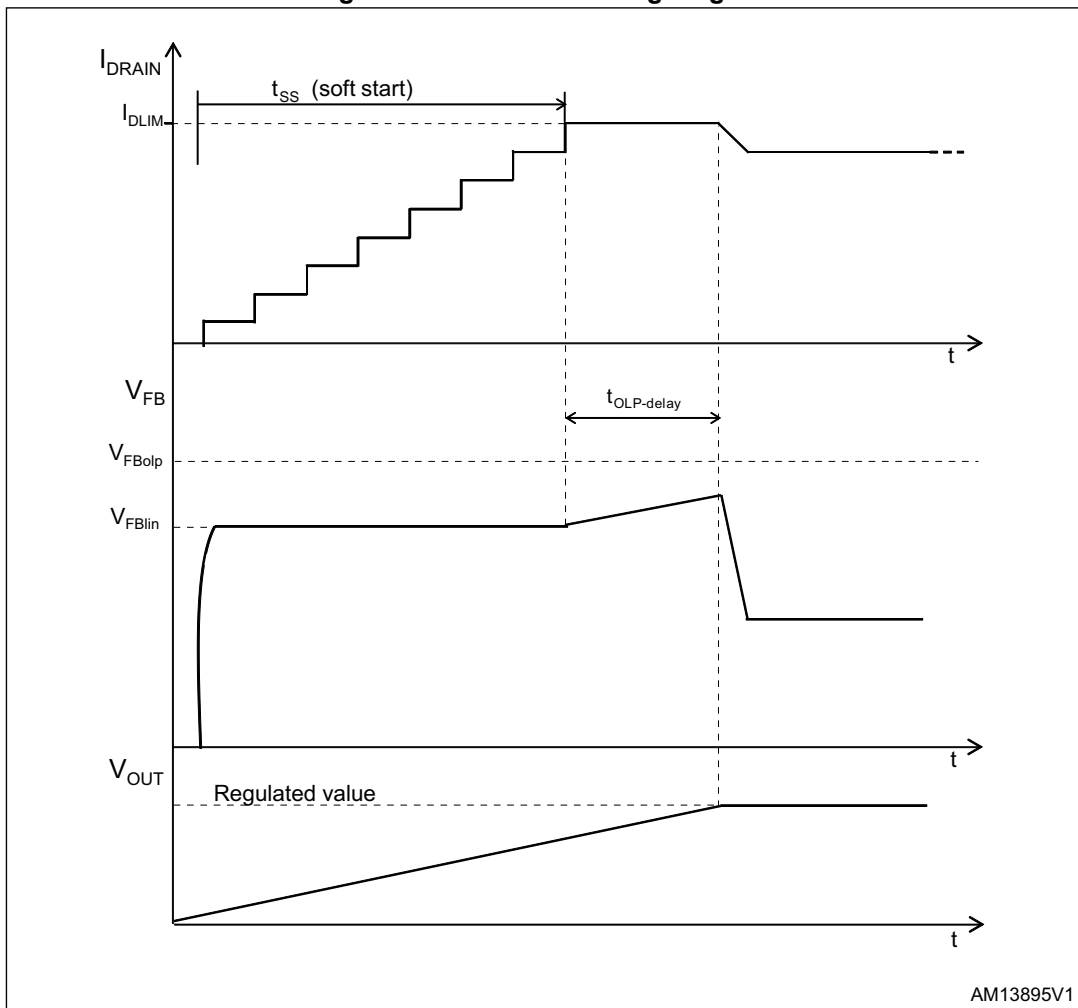


Figure 19. Soft-start: timing diagram



AM13895V1

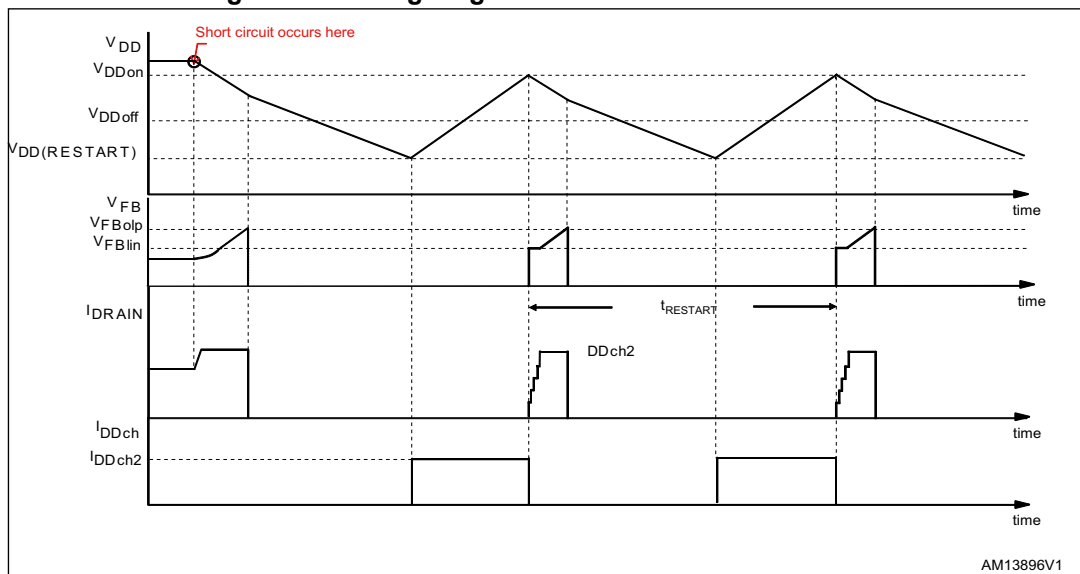
## 7.4 Power-down

At converter power-down, the system loses its ability to regulate as soon as the decreasing input voltage is low enough for the peak current limitation to be reached. The VDD voltage drops and when it falls below the  $V_{DD\text{off}}$  threshold (see [Table 7: Supply section](#)) the power MOSFET is switched OFF, the energy transfers to the IC is interrupted and, consequently, the VDD voltage decreases ([Table 19: Soft-start: timing diagram](#)), the startup sequence is inhibited and the power-down is completed. This feature is useful as it prevents the converter from attempting a restart and ensures monotonic output voltage decay during system power-down.

## 7.5 Auto-restart

Every time a protection is tripped, the IC is automatically restarted after a duration that depends on the discharge and recharge of the  $C_{VDD}$  capacitor. As shown in [Figure 20: Timing diagram: behavior after short-circuit](#), after a fault the IC is stopped and, consequently, the VDD voltage decreases because of the IC's consumption. As soon as the VDD voltage falls below the threshold  $V_{DD(\text{RESTART})}$  and if the DC input voltage is higher than  $V_{\text{DRAIN\_START}}$  threshold, the internal HV current source is turned ON and it starts to charge the  $C_{VDD}$  capacitor with the current  $I_{DD\text{ch2}}$  (0.6 mA, typ). As soon as the VDD voltage reaches the threshold  $V_{DD(\text{ON})}$ , the IC restarts.

**Figure 20. Timing diagram: behavior after short-circuit**



## 7.6 Oscillator

The switching frequency is internally fixed to 60 kHz or 115 kHz. In both cases the switching frequency is modulated by approximately  $\pm 4$  kHz (60 kHz version) or  $\pm 8$  kHz (115 kHz version) at 920 Hz (typical) rate, so that the resulting spread-spectrum action distributes the energy of each harmonic of the switching frequency over a number of side-band harmonics having the same energy on the whole, but smaller amplitudes.

## 7.7 Current mode conversion with adjustable current limit setpoint

The device is a current mode converter. The drain current is sensed and converted to voltage that is applied to the non-inverting pin of the PWM comparator. This voltage is compared with the one on the feedback pin through a voltage divider on a cycle-by-cycle basis.

The device has a default current limit value,  $I_{Dlim}$ , that can be adjusted according to the electrical specification, by the  $R_{LIM}$  resistor connected to the CONT pin.

The CONT pin has a minimum current sunk needed to activate the  $I_{Dlim}$  adjustment. Without  $R_{LIM}$  or with high  $R_{LIM}$  (i.e. 100 k $\Omega$ ) the current limit is set to the default value (see  $I_{Dlim}$ , [Table 8: Controller section](#)).

## 7.8 Overvoltage protection (OVP)

The device has an integrated logic for the monitoring of the output voltage using as an input signal the voltage VCONT during the OFF time of the power MOSFET. This is the time when the voltage from the auxiliary winding tracks the output voltage, through the turn ratio.

The CONT pin has to be connected to the auxiliary winding through the diode DOVP and the resistors ROVP and RLIM as shown in [Figure 22: CONT pin configuration](#). When, during the OFF time, the voltage VCONT exceeds four consecutive times the reference voltage VOVP (see [Table 8: Controller section](#)), the overvoltage protection will stop the power MOSFET and the converter enters auto-restart mode.

In order to bypass the noise immediately after the turn-off of the power MOSFET, the voltage VCONT is sampled inside a short window after the time TSTROBE, see [Table 8: Controller section](#) and the [Figure 21: OVP timing diagram](#). The sampled signal, if higher than VOVP, triggers the internal OVP digital signal and increments the internal counter. The same counter is reset every time the signal OVP is not triggered in one oscillator cycle.

Referring to [Figure 22: CONT pin configuration](#), once fixing RLIM according to the desired IDlim, the ROVP can be calculated by::

### Equation 2

$$R_{OVP} = \frac{(V_{OUTOVP} + V_{DSEC}) \cdot \frac{N_{AUX}}{N_{SEC}} - V_{OVP} - V_{DAUX}}{I_{CONT} + \frac{V_{OVP}}{R_{LIM}}}$$

Where:

- $V_{OVP}$  is the OVP threshold (see [Table 8: Controller section](#))
- $V_{OUTOVP}$  is the converter output voltage value to activate the OVP set by the designer
- $N_{AUX}$  is the number of the auxiliary winding turns
- $N_{SEC}$  is the number of the secondary winding turns
- $V_{DSEC}$  is the secondary diode forward voltage
- $V_{DAUX}$  is the auxiliary diode forward voltage

- $I_{CONT}$  is the current sunk by the CONT pin during the Mosfet off-time and is 10 $\mu$ A typical value.
- $R_{OVP}$  together with  $R_{LIM}$  constitute the output voltage divider

In the above formula, the effect of the not perfect coupling between the windings can be also considered, using the transformer's coupling parameter,  $K_T$ .

In this case the ratio  $N_{AUX}/N_{SEC}$  is replaced by the quantity  $K_T \cdot (N_{AUX}/N_{SEC})$ , where  $K_T$  is in the range 0.98-0.9, depending on the transformer's construction technique.

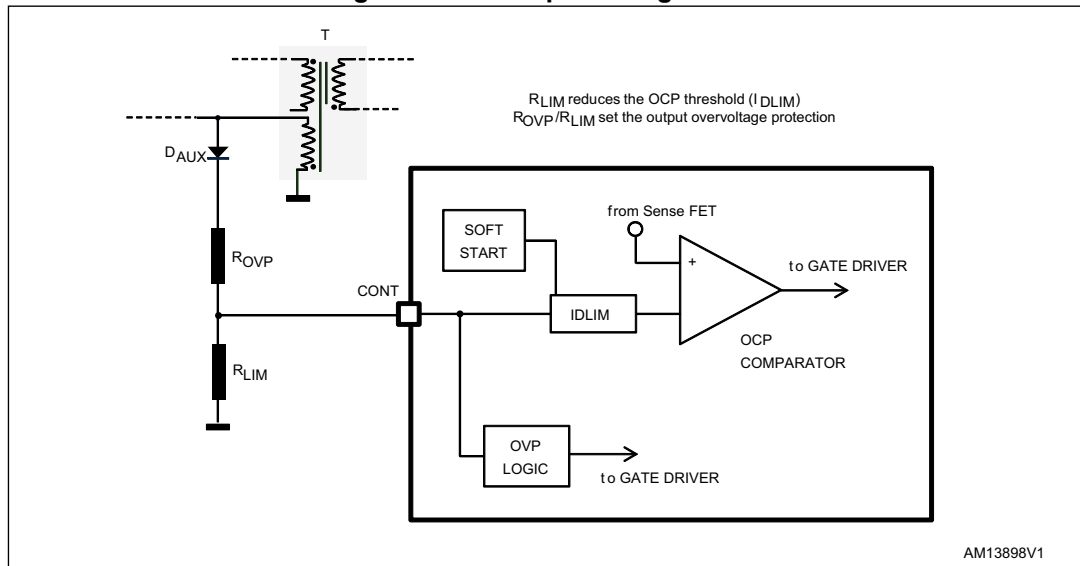
## 7.9 About CONT pin

Referring to [Figure 23](#), the CONT pin is used to configure the:

1. reduction of the OCP setpoint ( $I_{DLIM}$ )
2. output overvoltage protection (OVP)

[Table 10](#) lists the external components needed to activate one or more of the CONT pin functions.

**Figure 21. CONT pin configuration**



**Table 9. CONT pin configurations**

Function / component	$R_{LIM}$	$R_{OVP}$	$D_{AUX}$
$I_{Dlim}$ reduction	See <a href="#">Figure 13</a>	No	No
OVP	$\geq 80 \text{ k}\Omega$	See <a href="#">Equation 4</a>	Yes
$I_{Dlim}$ reduction and OVP <sup>(1)</sup>	See <a href="#">Figure 13</a>	See <a href="#">Equation 4</a>	Yes

1. Select  $R_{LIM}$  then  $R_{OVP}$ .

## 7.10 Feedback and overload protection (OLP)

The device is a current-mode converter. The feedback pin controls PWM operation as well as burst mode and activates the overload protection. [Figure 22: FB pin configuration \(option 1\)](#) and [Figure 23: FB pin configuration \(option 2\)](#) show the internal current-mode structure.

With the feedback pin voltage between  $V_{FBbm}$  and  $V_{FBlin}$ , (see [Table 8: Controller section](#)) the drain current is sensed and converted to voltage that is applied to the non-inverting pin of the PWM comparator.

This voltage is compared to the voltage on the feedback pin through a voltage divider on a cycle-by-cycle basis. When these two voltages are equal, the PWM logic orders the switch-off of the power MOSFET. The drain current is always limited to the value of  $I_{Dlim}$ .

When the feedback pin voltage reaches the threshold  $V_{FBlin}$ , an internal current generator starts to charge the feedback capacitor ( $C_{FB}$ ) and when the feedback voltage reaches the  $V_{FBolp}$  threshold, the converter is turned off and the automatic restart is activated.

During startup, when the output voltage is still low, if the feedback network is not properly dimensioned, the feedback voltage could rise up to the overload threshold ( $V_{FBolp}$ ) generating the switching off of the IC itself. Taking into account that the feedback network also fixes the loop stability, two options can be considered for this network.

The time from the overload detection ( $V_{FB} = V_{FBlin}$ ) to the device shutdown ( $V_{FB} = V_{FBolp}$ ) must be set by  $C_{FB}$  (or  $C_{FB1}$ ) using the formula:

### Equation 3

$$T_{OLP\_delay} = C_{FB} \times \frac{V_{FBolp} - V_{FBlin}}{I_{FB2}}$$

In the option 1 shown in [Figure 22: FB pin configuration \(option 1\)](#), the capacitor  $C_{FB}$  has a dual function: guaranteeing the loop compensation and fixing the overload delay time as calculated in [Equation 3](#).

Owing to the above considerations, the OLP delay time must be long enough to bypass the initial output voltage transient and check the overload condition only when the output voltage is in steady state. The output transient time depends on the value of the output capacitor and on the load.

When the value of the  $C_{FB}$  capacitor calculated for the loop stability is too low and cannot ensure enough OLP delay, an alternative compensation network can be used and it is shown in [Figure 23: FB pin configuration \(option 2\)](#).

Using this alternative compensation network, two poles ( $f_{PFB}$ ,  $f_{PFB1}$ ) and one zero ( $f_{ZFB}$ ) are introduced by the capacitors  $C_{FB}$  and  $C_{FB1}$  and the resistor  $R_{FB1}$ .

The capacitor  $C_{FB}$  introduces a pole ( $f_{PFB}$ ) at higher frequency than  $f_{ZB}$  and  $f_{PFB1}$ . This pole is usually used to compensate the high-frequency zero due to the ESR (equivalent series resistor) of the output capacitance of the flyback converter.

The mathematical expressions of these poles and zero frequency are:

$$f_{ZFB} = \frac{1}{2 \cdot \pi \cdot C_{FB1} \cdot R_{FB1}}$$

## Equation 4

$$f_{PFB} = \frac{R_{FB(DYN)} + R_{FB1}}{2 \cdot \pi \cdot C_{FB} \cdot (R_{FB(DYN)} \cdot R_{FB1})}$$

## Equation 5

$$f_{FB1} = \frac{1}{2 \cdot \pi \cdot C_{FB1} \cdot (R_{FB1} + R_{FB(DYN)})}$$

The  $R_{FB(DYN)}$  is the dynamic resistance seen by the FB pin.

The  $C_{FB1}$  capacitor fixes the OLP delay and usually  $C_{FB1}$  results in a much higher value than  $C_{FB}$ . Equation 3 can be still used to calculate the OLP delay, but  $C_{FB1}$  has to be considered instead of  $C_{FB}$ . Using the compensation network shown in option 2, in all cases the loop stability can be set as well as a sufficient OLP delay.

Figure 22. FB pin configuration (option 1)

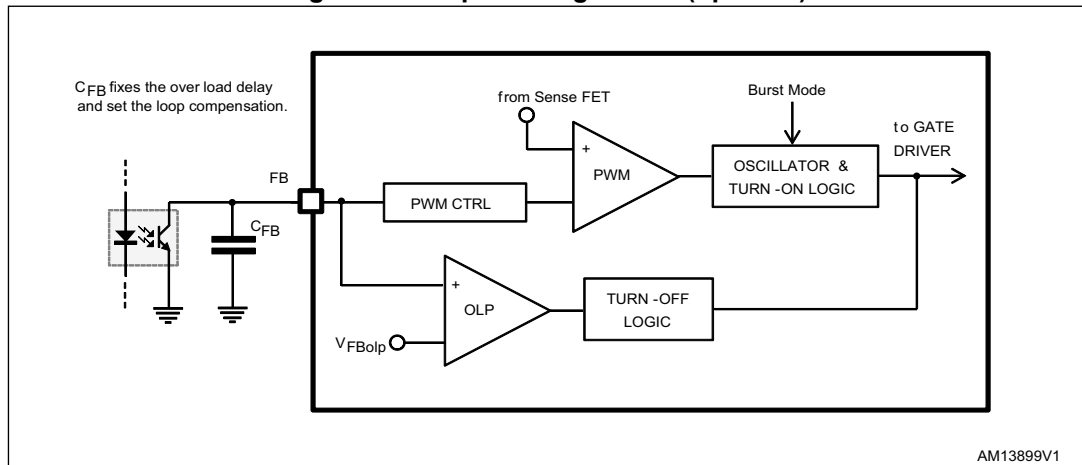
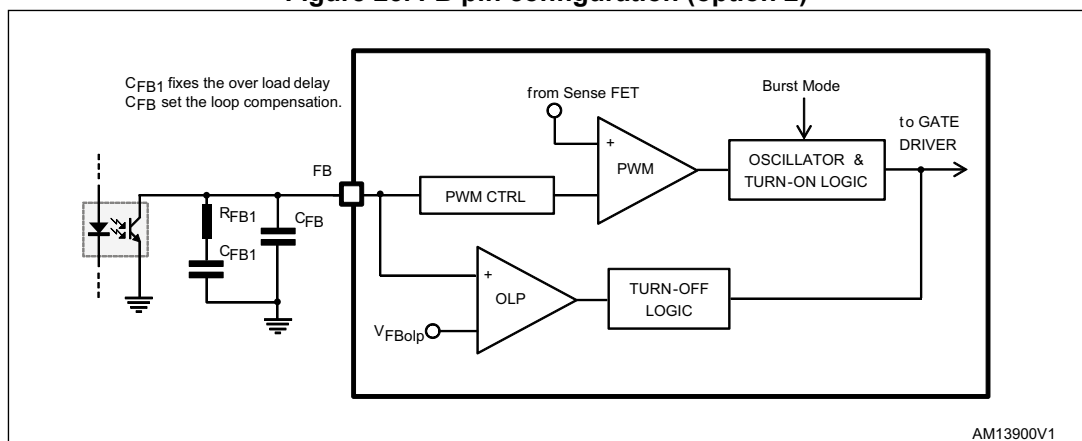


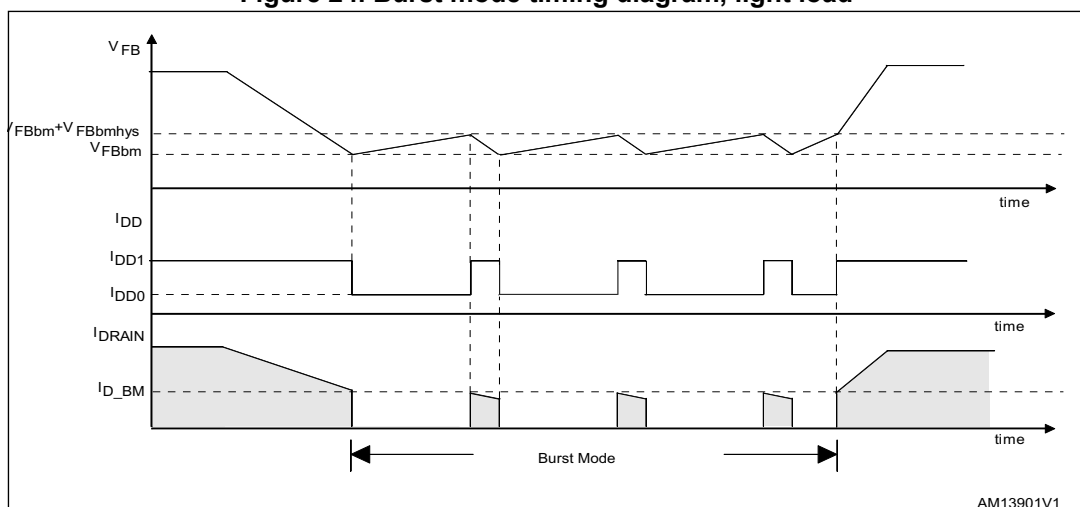
Figure 23. FB pin configuration (option 2)



## 7.11 Burst-mode operation at no load or very light load

When the load decreases, the feedback loop reacts by lowering the feedback pin voltage. If it falls below the burst mode threshold,  $V_{FBbm}$ , the power MOSFET is no longer allowed to be switched on. After the MOSFET stops, the feedback pin voltage increases and when it exceeds the level,  $V_{FBbm} + V_{FBbmhys}$ , the power MOSFET starts switching again. The burst mode thresholds are provided in [Table 8: Controller section](#) and [Figure 24: Burst mode timing diagram, light load](#) shows this behavior. The system alternates between a period of time where the power MOSFET is switching to a period of time where the power MOSFET is not switching. This mode of operation is the burst mode. The advantage of burst mode operation is an average switching frequency much lower than the normal operation frequency, up to several hundred hertz, minimizing all frequency-related losses. In order to prevent audible noise, during burst mode the drain current peak is clamped to the level,  $I_{D\_BM}$ , given in [Table 8: Controller section](#).

Figure 24. Burst mode timing diagram, light load



## 7.12 Extra power timer (EPT)

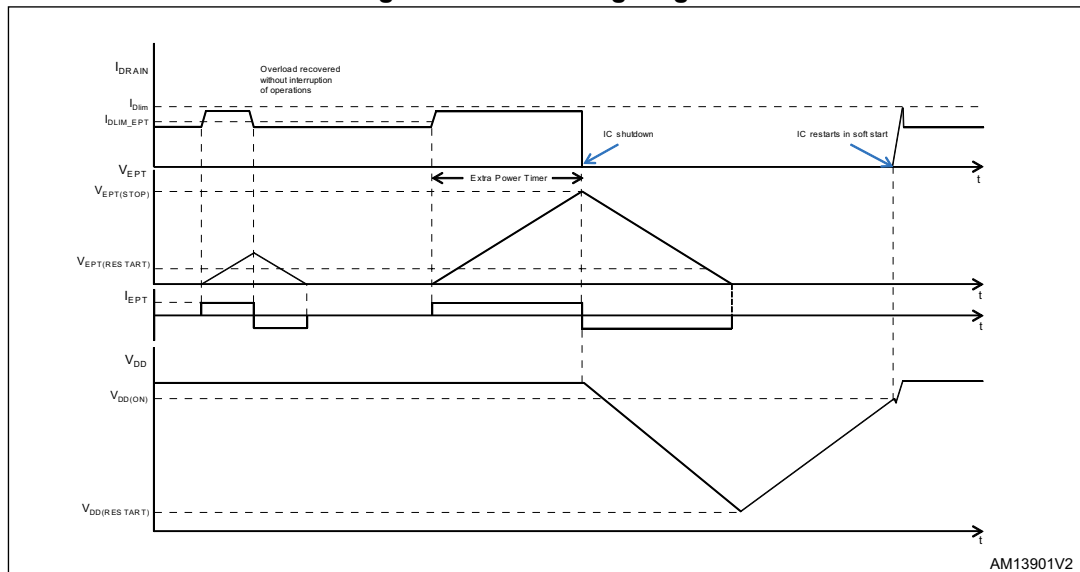
The extra power timer feature allows the setting of a blanking time inside which an overload current can be admitted. The timer is set through a capacitor ( $C_{EPT}$ ) connected to the EPT pin. Its duration is in the range of a few seconds and is limited by thermal constraints.

The extra power timer (EPT) is started as soon as the drain current reaches the threshold  $I_{DLIM\_EPT}$  (typ. 85% of  $I_{Dlim}$ ) and its duration is defined by the time needed to charge the capacitor  $C_{EPT}$  up to the value  $V_{EPT(STOP)}$  (4V, typ). The charging current is  $I_{EPT}$  (5 uA, typ).

If the EPT starts, the IC sustains the overload and continues to operate normally if the drain current falls below the threshold  $I_{DLIM\_EPT}$  (85% of  $I_{Dlim}$ ) before the EPT voltage reaches the value  $V_{EPT(STOP)}$ . The capacitor  $C_{EPT}$  is discharged through the current  $I_{EPT}$  (5 uA, typ) and the next EPT is inhibited until the EPT voltage is higher than  $V_{EPT(RESTART)}$  (0.6 V, typ). If the EPT starts and the EPT voltage reaches the value  $V_{EPT(STOP)}$ , the IC stops and it is automatically restarted. The  $C_{VDD}$  capacitor is then discharged down to the value  $V_{DD(RESTART)}$  (4.5 V, typ) and is recharged, through the HV current source, up to the value  $V_{DDon}$  (14 V, typ). Also in this case the capacitor  $C_{EPT}$  is discharged through the  $I_{EPT}$  current. See [Figure 25: EPT timing diagram](#) and [Table 7: Supply section](#). The EPT pin has

to be connected to GND if the function is not used.

Figure 25. EPT timing diagram



## 7.13 2<sup>nd</sup> level overcurrent protection and hiccup mode

The device is protected against short-circuit of the secondary rectifier, short-circuit on the secondary winding or a hard-saturation of the flyback transformer. This type of anomalous condition is invoked when the drain current exceeds the threshold  $I_{D_{MAX}}$ , see [Table 8: Controller section](#).

To distinguish a real malfunction from a disturbance (e.g. induced during ESD tests) a "warning state" is entered after the first signal is tripped. If, in the subsequent switching cycles, the signal is not tripped, a temporary disturbance is assumed and the protection logic will be reset in its idle state; otherwise if the  $I_{D_{MAX}}$  threshold is exceeded for two consecutive switching cycles, a real malfunction is assumed and the power MOSFET is turned OFF.

The shutdown condition is latched as long as the device is supplied. While it is disabled, no energy is transferred from the auxiliary winding, hence the voltage on the  $C_{VDD}$  capacitor decays until the  $V_{DD}$  undervoltage threshold ( $V_{DDoff}$ ), which clears the latch.

The startup HV current generator is still off, until the  $V_{DD}$  voltage falls below its restart voltage,  $V_{DD(RESTART)}$ . After this condition the  $C_{VDD}$  capacitor is charged again by the  $I_{DDch2}$  current, and the converter switching restarts if  $V_{DDon}$  occurs. If the fault condition is not removed, the device enters auto-restart mode. This behavior results in a low-frequency intermittent operation (hiccup-mode operation), with very low stress on the power circuit.

## 8 Package information

In order to meet environmental requirements, ST offers these devices in different grades of ECOPACK<sup>®</sup> packages, depending on their level of environmental compliance. ECOPACK<sup>®</sup> specifications, grade definitions and product status are available at: [www.st.com](http://www.st.com). ECOPACK<sup>®</sup> is an ST trademark.

### 8.1 SDIP10 package information

Figure 26. SDIP10 package outline

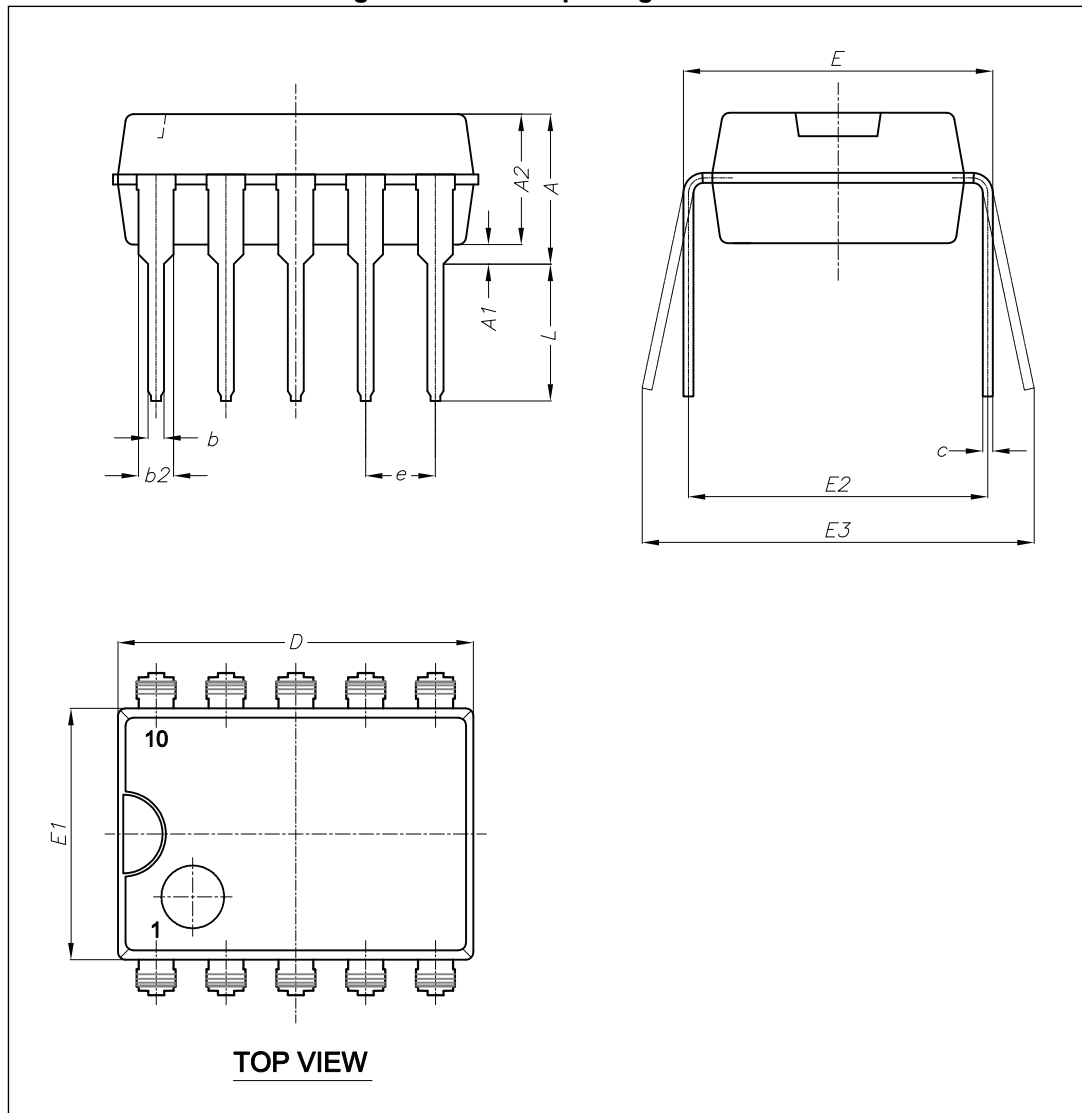


Table 10. SDIP10 mechanical data

Dim.	mm		
	Min.	Typ.	Max.
A			5.33
A1	0.38		
A2	2.92		4.95
b	0.36		0.56
b2	0.51		1.15
c	0.2		0.36
D	9.02		10.16
E	7.62		8.26
E1	6.1		7.11
E2		7.62	
E3			10.92
e		1.77	
L	2.92		3.81

## 8.2 SO16 Narrow package information

Figure 27. SO16 Narrow package outline

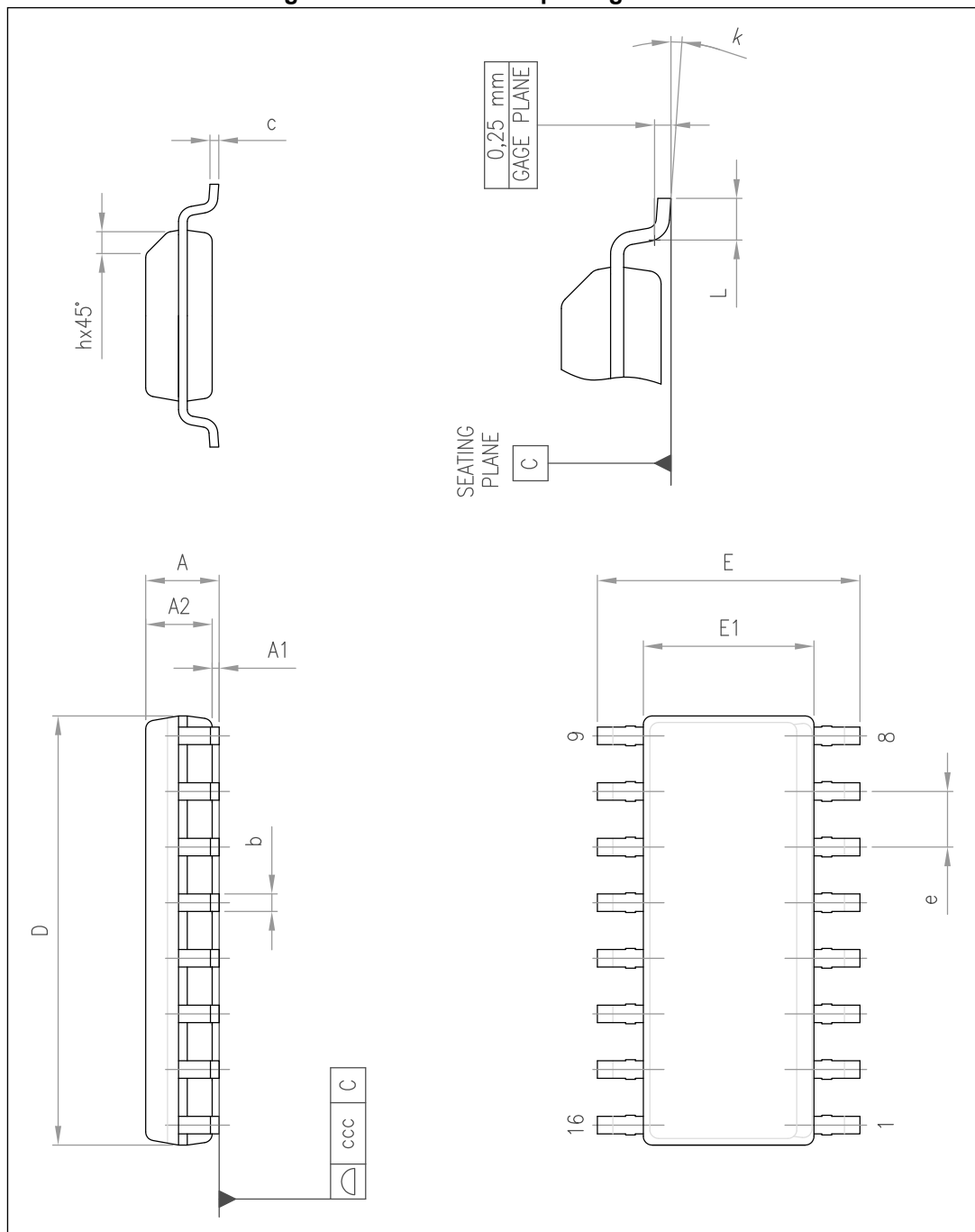


Table 11. SO16 Narrow mechanical data

Dim.	mm		
	Min.	Typ.	Max.
A			1.75
A1	0.1		0.25
A2	1.25		
b	0.31		0.51
c	0.17		0.25
D	9.8	9.9	10
E	5.8	6	6.2
E1	3.8	3.9	4
e		1.27	
h	0.25		0.5
L	0.4		1.27
k	0		8
ccc			0.1

## 9 Order code

**Table 12. Order code**

Order code	Package	Packing
VIPER38LE	SDIP10	Tube
VIPER38HE		
VIPER38HD	SO16 narrow	Tape and reel
VIPER38LD		
VIPER38HDTR		
VIPER38LDTR		

## 10 Revision history

**Table 13. Document revision history**

Date	Revision	Changes
19-Mar-2014	1	Initial release
14-Jul-2015	2	Updated title, features and description in cover page. Added SO16 narrow package. Removed Device summary table. Updated <i>Section 2: Typical power</i> , <i>Section 3: Pin settings</i> , and <i>Section 7: Operation</i> . Added <i>Section 8.2: SO16 Narrow package information</i> and <i>Section 9: Order code</i> . Minor text changes.
06-Nov-2019	3	Modified <i>Table 4: Thermal data</i> . Updated content of <i>Section 7.8: Overvoltage protection (OVP)</i>

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