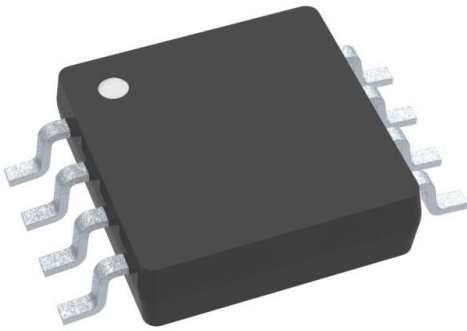


INA310B3QDGKRQ1 Datasheet

www.digi-electronics.com



<https://www.DiGi-Electronics.com>

| | |
|------------------------------|---|
| DiGi Electronics Part Number | INA310B3QDGKRQ1-DG |
| Manufacturer | Texas Instruments |
| Manufacturer Product Number | INA310B3QDGKRQ1 |
| Description | AEC-Q100 -4-V TO 110-V 1.3-MHZ H |
| Detailed Description | Current Sense Amplifier 1 Circuit Single-Ended 8-VS SOP |



Tel: +00 852-30501935

RFQ Email: Info@DiGi-Electronics.com

DiGi is a global authorized distributor of electronic components.

Purchase and inquiry

Manufacturer Product Number:

INA310B3QDGKRQ1

Series:

-

Amplifier Type:

Current Sense

Output Type:

Single-Ended

-3db Bandwidth:

1 MHz

Voltage - Input Offset:

30 μ V

Voltage - Supply Span (Min):

2.7 V

Operating Temperature:

-40°C ~ 125°C (TA)

Qualification:

AEC-Q100

Package / Case:

8-TSSOP, 8-MSOP (0.118", 3.00mm Width)

Manufacturer:

Texas Instruments

Product Status:

Active

Number of Circuits:

1

Slew Rate:

2.5V/ μ s

Current - Input Bias:

20 μ A

Current - Supply:

1.6mA

Voltage - Supply Span (Max):

20 V

Grade:

Automotive

Mounting Type:

Surface Mount

Supplier Device Package:

8-VSSOP

Environmental & Export classification

RoHS Status:

ROHS3 Compliant

REACH Status:

REACH Unaffected

HTSUS:

8542.39.0001

Moisture Sensitivity Level (MSL):

2 (1 Year)

ECCN:

EAR99

INA310x-Q1 AEC-Q100, –4 V to 110 V, 1.3 MHz, Ultra-Precise Current Sense Amplifier With Open-Drain Comparator and Reference

1 Features

- AEC-Q100 qualified for automotive applications:
 - Temperature grade 1: –40°C to +125°C, T_A
- **Functional Safety-Capable**
 - [Documentation available to aid functional safety system design](#)
- Wide common-mode voltage:
 - Operational voltage: –4 V to +110 V
 - Survival voltage: –20 V to +120 V
- High signal bandwidth: 1.3 MHz
- Slew rate: 2.5 V/μs
- Excellent CMRR: 160 dB
- Accuracy
 - Gain error (maximum)
 - Version A: 0.15%, 10 ppm/°C drift
 - Version B: 0.5%, 20 ppm/°C drift
 - Offset voltage (maximum)
 - Version A: ±20 μV, ±0.25 μV/°C drift
 - Version B: ±150 μV, ±1 μV/°C drift
- Onboard open-drain comparator
- Internal comparator voltage reference: 0.6 V
- Propagation delay time: 1 μs
- Latching capability on comparator
- Available gains:
 - INA310A1-Q1, INA310B1-Q1 : 20 V/V
 - INA310A2-Q1, INA310B2-Q1 : 50 V/V
 - INA310A3-Q1, INA310B3-Q1 : 100 V/V
 - INA310A4-Q1, INA310B4-Q1 : 200 V/V
 - INA310A5-Q1, INA310B5-Q1 : 500 V/V
- Package options: VSSOP-8

2 Applications

- [eTurbo/charger](#)
- [Electric power steering \(EPS\)](#)
- [Starter/generator](#)
- [Regenerative braking](#)
- [Brake system](#)

3 Description

The INA310x-Q1 is an ultra-precise current sense amplifier that can measure voltage drops across shunt resistors over a wide common-mode range from –4 V to 110 V, independent of supply voltage with an integrated comparator. The high precision current measurement accuracy is achieved through a combination of low offset voltage (20 μV, maximum), small gain error (0.15%, maximum) and a high DC CMRR (160 dB, typical). The INA310x-Q1 has a high signal bandwidth of 1.3 MHz designed for high voltage DC current measurements and high-speed applications like fast overcurrent protection.

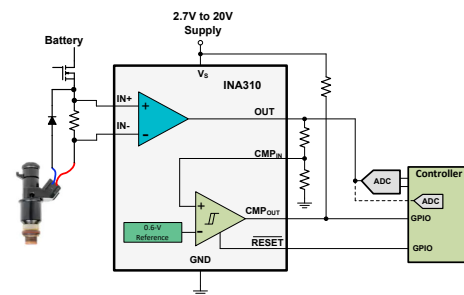
The INA310x-Q1 incorporates an open-drain comparator and internal reference that provides a 0.6 V threshold. An external resistive divider sets the current trip point. The comparator includes a latching capability that can be made transparent by grounding (or leaving open) the $\overline{\text{RESET}}$ pin.

The INA310x-Q1 operates from a single 2.7 V to 20 V supply and draws 1.6 mA of supply current. The INA310x-Q1 is available in five gain options: 20 V/V, 50 V/V, 100 V/V, 200 V/V, and 500 V/V. These gain options address a wide dynamic range of current-sensing applications.

Package Information

| PART NUMBER | PACKAGE ⁽¹⁾ | PACKAGE SIZE ⁽²⁾ |
|-------------|------------------------|-----------------------------|
| INA310A-Q1 | VSSOP (8) | 3.00 mm × 4.90 mm |
| INA310B-Q1 | | |

- (1) For all available packages, see the orderable addendum at the end of the data sheet.
- (2) The package size (length × width) is a nominal value and includes pins, where applicable.



Typical Application

Table of Contents

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4 Revision History

| DATE | REVISION | NOTES |
|----------|----------|-----------------|
| May 2023 | * | Initial release |

5 Pin Configuration and Functions

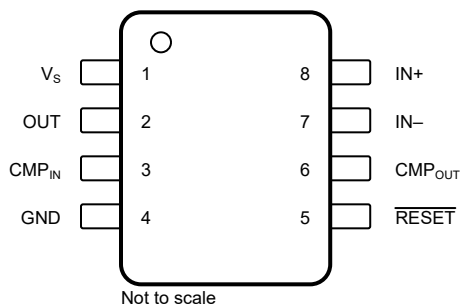


Figure 5-1. INA310x-Q1: DGK Package 8-Pin VSSOP Top View

Table 5-1. Pin Functions

| PIN | | TYPE | DESCRIPTION |
|--------------------|----|--------|--|
| NAME | NO | | |
| V _S | 1 | Power | Power supply, 2.7 V to 20 V |
| OUT | 2 | Output | Output voltage |
| CMP _{IN} | 3 | Input | Comparator input |
| GND | 4 | Ground | Ground |
| RESET | 5 | Input | Comparator reset pin, active low (Low: Transparent Mode, High: Latch Mode) |
| CMP _{OUT} | 6 | Output | Comparator output (latch high when RESET = High) |
| IN ₋ | 7 | Input | Shunt resistor negative sense input. For high-side applications, connect to load side of sense resistor. For low-side applications, connect to ground side of sense resistor. |
| IN ₊ | 8 | Input | Shunt resistor positive sense input. For high-side applications, connect to bus-voltage side of sense resistor. For low-side applications, connect to load side of sense resistor. |

INA310A-Q1, INA310B-Q1

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6 Specifications**6.1 Absolute Maximum Ratings**over operating free-air temperature range (unless otherwise noted)⁽¹⁾

| | | MIN | MAX | UNIT | |
|-------------------------------------|----------------------------|--|------------------------------|------|---|
| V _S | Supply voltage | -0.3 | 22 | V | |
| V _{IN+} , V _{IN-} | Analog inputs | Differential (V _{IN+}) – (V _{IN-}) ⁽²⁾ | -12 | 12 | V |
| | | V _{IN+} , V _{IN-} , with respect to GND ⁽²⁾ | -20 | 120 | |
| V _{OUT} | Analog output | GND – 0.3 | (V _S) + 0.3 | V | |
| | Comparator reset pin | GND – 0.3 | (V _S) + 0.3 | V | |
| | Comparator analog input | GND – 0.3 | MIN of 5.5 or V _S | V | |
| | Comparator Output | GND – 0.3 | 22 | V | |
| | Input current into any pin | | 5 | mA | |
| T _A | Operating temperature | -55 | 150 | °C | |
| T _J | Junction temperature | -65 | 150 | °C | |
| T _{stg} | Storage temperature | -65 | 150 | °C | |

- (1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- (2) V_{IN+} and V_{IN-} are the voltages at the IN+ and IN- pins, respectively.

6.2 ESD Ratings

| | | | VALUE | UNIT |
|--------------------|-------------------------|---|-------|------|
| V _(ESD) | Electrostatic discharge | Human body model (HBM), per AEC Q100-002 ⁽¹⁾ | ±2000 | V |
| | | Charged device model (CDM), per AEC Q100-011 | ±1000 | |

- (1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

| | | MIN | NOM | MAX | UNIT |
|--------------------|--------------------------------|-----|-----|--------------------|------|
| V _{CM} | Common-mode input range | -4 | 48 | 110 | V |
| V _S | Operating supply voltage | 2.7 | 5 | 20 | V |
| V _{SENSE} | Differential sense input range | 0 | | V _S / G | V |
| T _A | Operating free-air temperature | -40 | | 125 | °C |

6.4 Thermal Information

| THERMAL METRIC ⁽¹⁾ | | INA310x-Q1 | UNIT |
|-------------------------------|--|-------------|------|
| | | DGK (VSSOP) | |
| | | 8 PINS | |
| R _{θJA} | Junction-to-ambient thermal resistance | 172.2 | °C/W |
| R _{θJC(top)} | Junction-to-case (top) thermal resistance | 63.5 | °C/W |
| R _{θJB} | Junction-to-board thermal resistance | 93.8 | °C/W |
| Ψ _{JT} | Junction-to-top characterization parameter | 9.8 | °C/W |
| Ψ _{JB} | Junction-to-board characterization parameter | 92.2 | °C/W |

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

6.5 Electrical Characteristics

at $T_A = 25^\circ\text{C}$, $V_{\text{SENSE}} = V_{\text{IN}+} - V_{\text{IN}-} = 0.5\text{ V} / \text{Gain}$, $V_S = 5.0\text{ V}$, $V_{\text{CM}} = V_{\text{IN}-} = 48\text{ V}$, and $R_{\text{PULLUP}} = 5.1\text{ k}\Omega$ connected from CMP_{out} to V_S , (unless otherwise noted)

| PARAMETER | | CONDITIONS | MIN | TYP | MAX | UNIT |
|-----------------------|------------------------------------|--|-----|------------------------|-------------------------|------------------------------|
| INPUT | | | | | | |
| V_{CM} | Common-mode input range | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | -4 | | 110 | V |
| CMRR | Common-mode rejection ratio | INA310Ax-Q1, $V_{\text{IN}+} = -4\text{ V}$ to 110 V , $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | 140 | 160 | | dB |
| | | INA310Ax-Q1, $f = 50\text{ kHz}$ | | 85 | | |
| | | INA310Bx-Q1, $V_{\text{IN}+} = -4\text{ V}$ to 110 V , $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | 120 | 140 | | |
| | | INA310Bx-Q1, $f = 50\text{ kHz}$ | | 65 | | |
| V_{OS} | Offset voltage, RTI ⁽¹⁾ | INA310A1-Q1 | | ± 30 | ± 150 | μV |
| | | INA310B1-Q1 | | ± 100 | ± 500 | |
| | | INA310A2-Q1 | | ± 15 | ± 80 | |
| | | INA310B2-Q1 | | ± 55 | ± 300 | |
| | | INA310A3-Q1 | | ± 10 | ± 50 | |
| | | INA310B3-Q1 | | ± 30 | ± 250 | |
| | | INA310A4-Q1 | | ± 5 | ± 30 | |
| | | INA310B4-Q1 | | ± 30 | ± 200 | |
| | | INA310A5-Q1 | | ± 2 | ± 20 | |
| dV_{OS}/dT | Offset drift, RTI | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$, INA310A1-Q1, INA310A2-Q1, INA310A3-Q1 | | ± 0.05 | ± 0.5 | $\mu\text{V}/^\circ\text{C}$ |
| | | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$, INA310A4-Q1, INA310A5-Q1 | | ± 0.025 | ± 0.25 | |
| | | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$, INA310Bx-Q1 | | ± 0.1 | ± 1 | |
| PSRR | Power-supply rejection ratio, RTI | INA310A1-Q1, $2.7\text{ V} \leq V_S \leq 20\text{ V}$, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | ± 1 | ± 8 | $\mu\text{V}/\text{V}$ |
| | | INA310A2-Q1, INA310A3-Q1, $2.7\text{ V} \leq V_S \leq 20\text{ V}$, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | ± 0.3 | ± 3 | |
| | | INA310A4-Q1, INA310A5-Q1, $2.7\text{ V} \leq V_S \leq 20\text{ V}$, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | ± 0.1 | ± 1 | |
| | | INA310Bx-Q1 $2.7\text{ V} \leq V_S \leq 20\text{ V}$, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | ± 1.5 | ± 10 | |
| I_B | Input bias current | I_{B+} , I_{B-} , $V_{\text{SENSE}} = 0\text{ mV}$ | 10 | 20 | 30 | μA |
| OUTPUT | | | | | | |
| G | Gain | INA310A1-Q1, INA310B1-Q1 | | 20 | | V/V |
| | | INA310A2-Q1, INA310B2-Q1 | | 50 | | |
| | | INA310A3-Q1, INA310B3-Q1 | | 100 | | |
| | | INA310A4-Q1, INA310B4-Q1 | | 200 | | |
| | | INA310A5-Q1, INA310B5-Q1 | | 500 | | |
| G_{ERR} | Gain error | INA310Ax-Q1, $\text{GND} + 50\text{ mV} \leq V_{\text{OUT}} \leq V_S - 200\text{ mV}$ | | $\pm 0.02\%$ | $\pm 0.15\%$ | $\text{ppm}/^\circ\text{C}$ |
| | | INA310Bx-Q1, $\text{GND} + 50\text{ mV} \leq V_{\text{OUT}} \leq V_S - 200\text{ mV}$ | | $\pm 0.07\%$ | $\pm 0.5\%$ | |
| | | INA310Ax-Q1, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | 1 | 10 | |
| | | INA310Bx-Q1, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | 2 | 20 | |
| NLERR | Nonlinearity error | $\text{GND} + 50\text{ mV} \leq V_{\text{OUT}} \leq V_S - 200\text{ mV}$ | | ± 0.01 | | % |
| | Maximum capacitive load | No sustained oscillation, no isolation resistor | | 500 | | pF |
| VOLTAGE OUTPUT | | | | | | |
| V_{SP} | Swing to V_S (Power-supply rail) | $R_{\text{LOAD}} = 10\text{ k}\Omega$ to GND, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | $(V_S) - 70$ | $(V_S) - 150$ | mV |
| V_{SN} | Swing to GND | $R_{\text{LOAD}} = 10\text{ k}\Omega$ to GND, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$, $V_{\text{SENSE}} = 0\text{ mV}$ | | $(V_{\text{GND}}) + 5$ | $(V_{\text{GND}}) + 20$ | mV |

INA310A-Q1, INA310B-Q1

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at $T_A = 25^\circ\text{C}$, $V_{\text{SENSE}} = V_{\text{IN}+} - V_{\text{IN}-} = 0.5\text{ V}$ / Gain, $V_S = 5.0\text{ V}$, $V_{\text{CM}} = V_{\text{IN}-} = 48\text{ V}$, and $R_{\text{PULLUP}} = 5.1\text{ k}\Omega$ connected from CMP_{out} to V_S , (unless otherwise noted)

| PARAMETER | | CONDITIONS | MIN | TYP | MAX | UNIT |
|---------------------------|--|---|-----|------|------|------------------------|
| FREQUENCY RESPONSE | | | | | | |
| BW | Bandwidth | INA310A1-Q1, INA310B1-Q1, $C_{\text{LOAD}} = 5\text{ pF}$, $V_{\text{SENSE}} = 200\text{mV}$ | | 1300 | | kHz |
| | | INA310A2-Q1, INA310B2-Q1, $C_{\text{LOAD}} = 5\text{ pF}$, $V_{\text{SENSE}} = 80\text{mV}$ | | 1300 | | |
| | | INA310A3-Q1, INA310B3-Q1, $C_{\text{LOAD}} = 5\text{ pF}$, $V_{\text{SENSE}} = 40\text{mV}$ | | 1000 | | |
| | | INA310A4-Q1, INA310B4-Q1, $C_{\text{LOAD}} = 5\text{ pF}$, $V_{\text{SENSE}} = 20\text{mV}$ | | 900 | | |
| | | INA310A5-Q1, INA310B5-Q1, $C_{\text{LOAD}} = 5\text{ pF}$, $V_{\text{SENSE}} = 8\text{mV}$ | | 900 | | |
| SR | Slew rate | Rising edge | | 2.5 | | V/ μs |
| t_S | Settling time | $V_{\text{OUT}} = 4\text{ V} \pm 0.1\text{ V}$ step, Output settles to 0.5% | | 10 | | μs |
| | | $V_{\text{OUT}} = 4\text{ V} \pm 0.1\text{ V}$ step, Output settles to 1% | | 5 | | μs |
| | | $V_{\text{OUT}} = 4\text{ V} \pm 0.1\text{ V}$ step, Output settles to 5% | | 1 | | μs |
| NOISE | | | | | | |
| V_{en} | Voltage noise density | | | 50 | | nV/ $\sqrt{\text{Hz}}$ |
| COMPARATOR | | | | | | |
| $V_{\text{THRESHOLD}}$ | Alert threshold | $T_A = 25^\circ\text{C}$ | 585 | 600 | 615 | mV |
| | | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | 580 | | 620 | mV |
| | Hysteresis | $T_A = 25^\circ\text{C}$ | | 8 | | mV |
| t_P | Small-signal propagation delay | Comparator input overdrive = 20 mV | | 1 | | μs |
| | Slew-rate-limited propagation delay | V_{OUT} step = 0.5 V to 4.5 V, $V_{\text{LIMIT}}^{(3)} = 4\text{ V}$ | | 1.6 | | μs |
| I_{BCMPIN} | Input bias current, CMP_{in} PIN | $T_A = 25^\circ\text{C}$, $V_{\text{CMPIN}} = 0.4\text{ V}$ to 1.2 V | -20 | 1 | 20 | nA |
| | | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$, $V_{\text{CMPIN}} = 0.4\text{ V}$ to 1.2 V | | | 250 | nA |
| I_{LKG} | High-level leakage current | $V_{\text{CMPout}} = V_S$ | | | 1 | μA |
| V_{OL} | Low-level output voltage | $I_{\text{OL}} = 2.35\text{ mA}$ | | | 300 | mV |
| | | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$, $I_{\text{OL}} = 2.35\text{ mA}$ | | | 350 | mV |
| V_{IH} | RESET High-level input voltage threshold (2) | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | 1.2 | | | V |
| V_{IL} | RESET Low-level input voltage threshold (2) | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | | 0.4 | V |
| | Minimum RESET pulse width | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | 100 | 200 | ns |
| | RESET propagation delay | | | 250 | | ns |
| POWER SUPPLY | | | | | | |
| V_S | Supply voltage range | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | 2.7 | | 20 | V |
| I_Q | Quiescent current | | | 1.6 | 2 | mA |
| | | $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$ | | | 2.25 | mA |

(1) RTI = referred-to-input.

(2) The RESET input has an internal 2 M Ω (typical) pulldown. Leaving RESET open results in a LOW state, with transparent comparator operation.

(3) V_{LIMIT} is V_{OUT} at the overcurrent threshold set by external resistors.

6.6 Typical Characteristics

at $T_A = 25^\circ\text{C}$, $V_S = 5\text{ V}$, $V_{\text{SENSE}} = V_{\text{IN}+} - V_{\text{IN}-} = 0.5\text{ V} / \text{Gain}$, $V_{\text{CM}} = V_{\text{IN}-} = 48\text{ V}$, and $R_{\text{PULLUP}} = 5.1\text{ k}\Omega$ (unless otherwise noted).

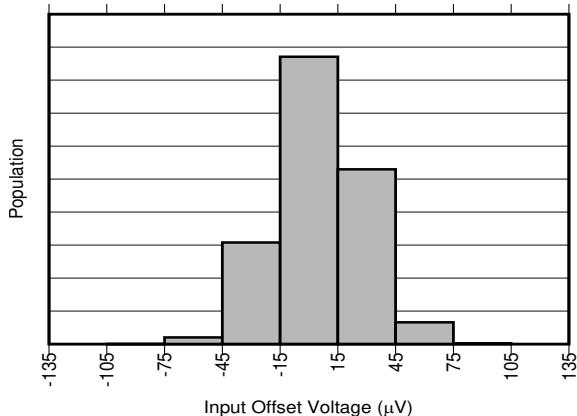


Figure 6-1. INA310A1-Q1 Input Offset Production Distribution

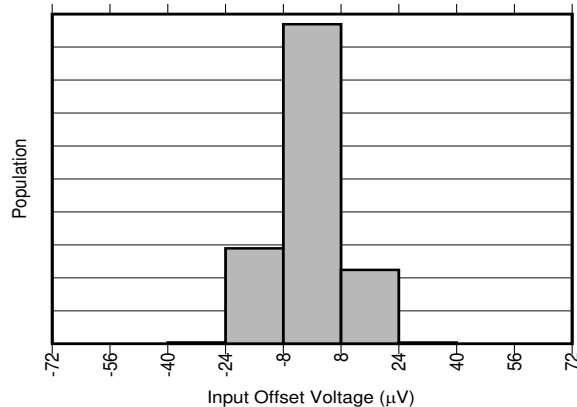


Figure 6-2. INA310A2-Q1 Input Offset Production Distribution

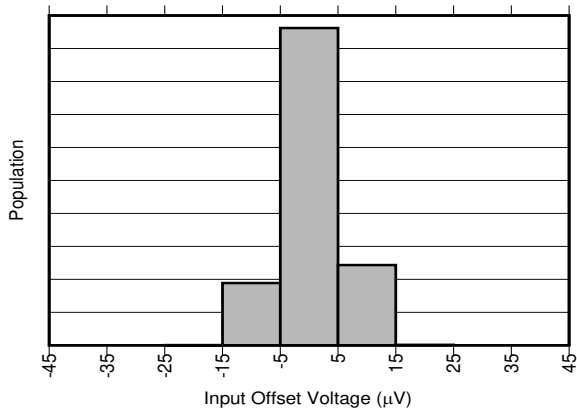


Figure 6-3. INA310A3-Q1 Input Offset Production Distribution

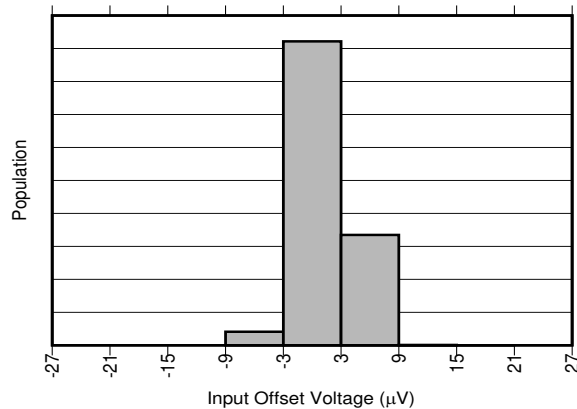


Figure 6-4. INA310A4-Q1 Input Offset Production Distribution

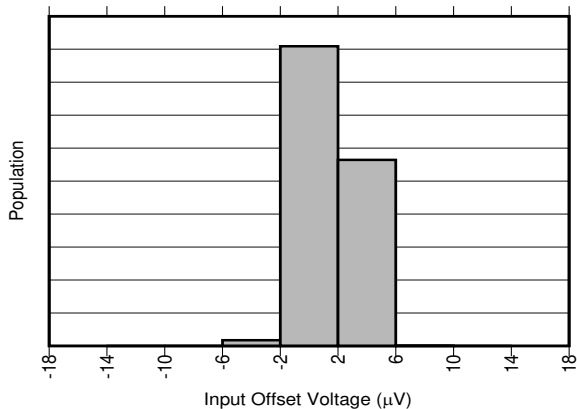


Figure 6-5. INA310A5-Q1 Input Offset Production Distribution

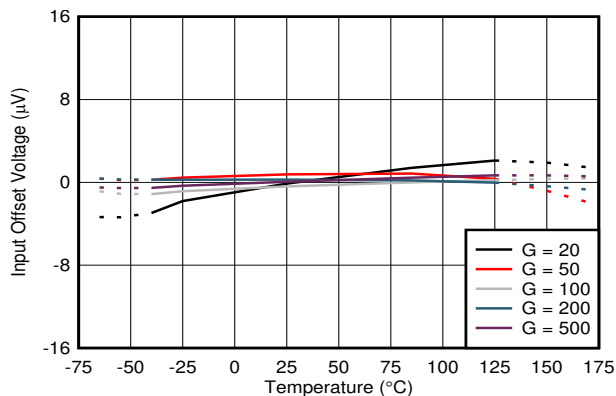


Figure 6-6. Input Offset Voltage vs Temperature

INA310A-Q1, INA310B-Q1

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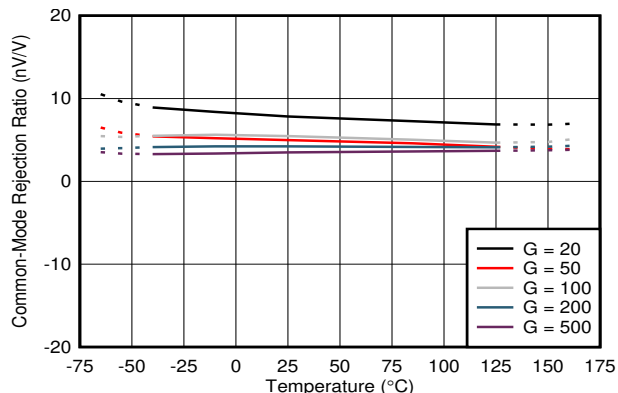


Figure 6-7. Common-Mode Rejection Ratio vs Temperature

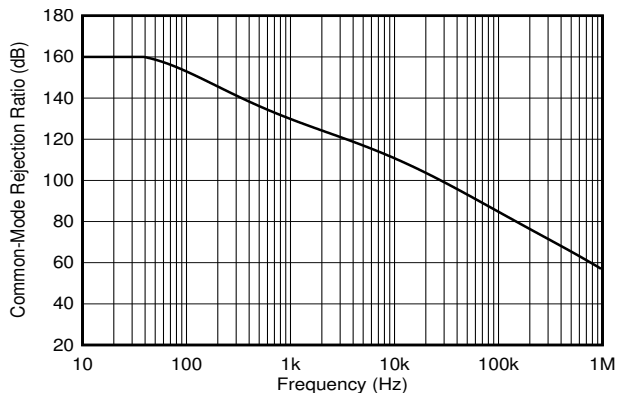


Figure 6-8. Common-Mode Rejection Ratio vs Frequency

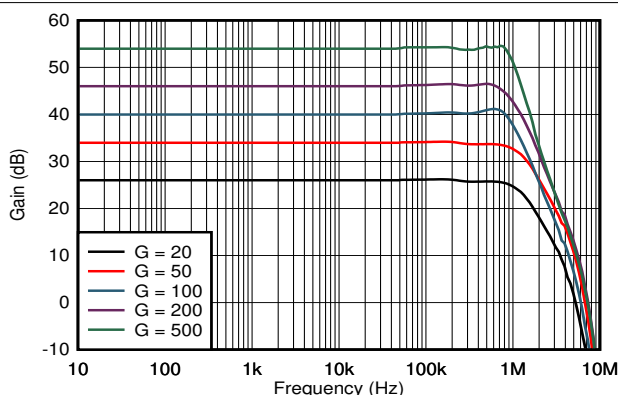


Figure 6-9. Gain vs Frequency

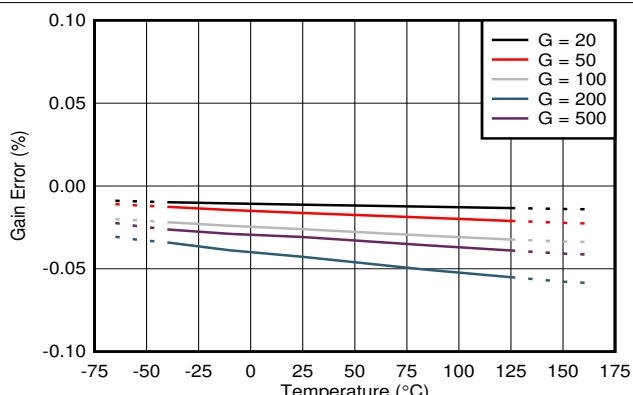


Figure 6-10. INA310A-Q1 Gain Error vs Temperature

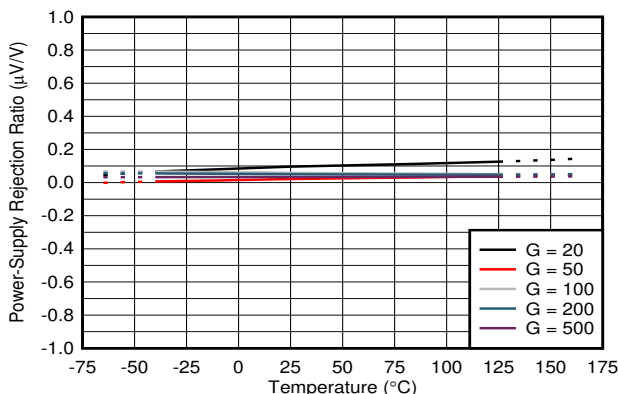


Figure 6-11. Power-Supply Rejection Ratio vs Temperature

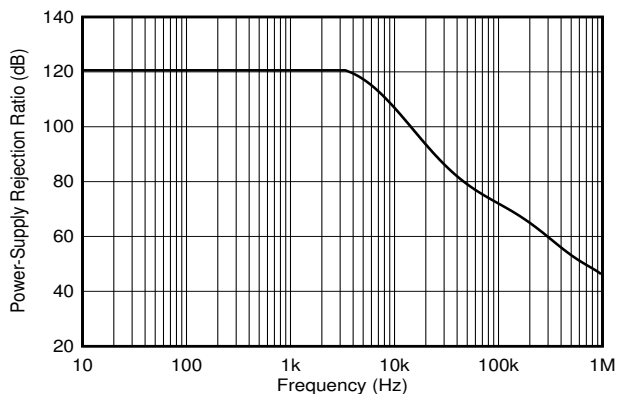


Figure 6-12. Power-Supply Rejection Ratio vs Frequency

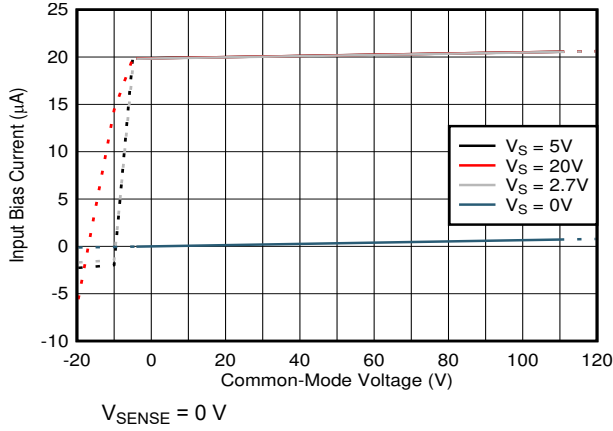


Figure 6-13. Input Bias Current vs Common-Mode Voltage

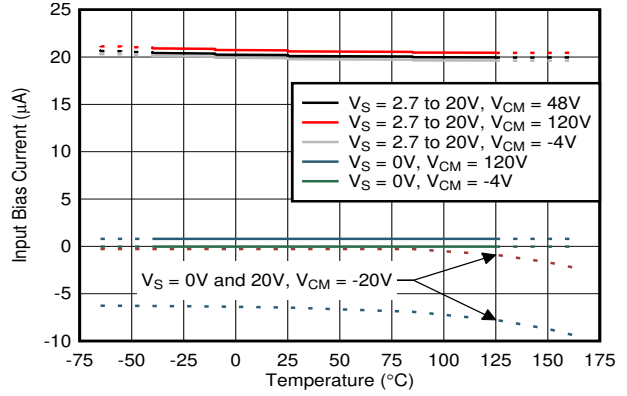


Figure 6-14. Input Bias Current vs Temperature

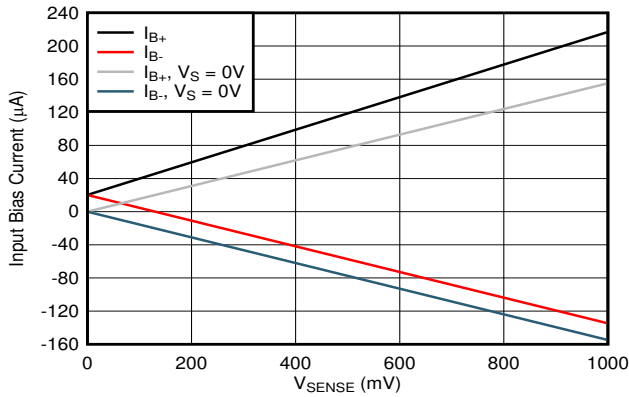


Figure 6-15. INA310x1-Q1 Input Bias Current vs VSENSE

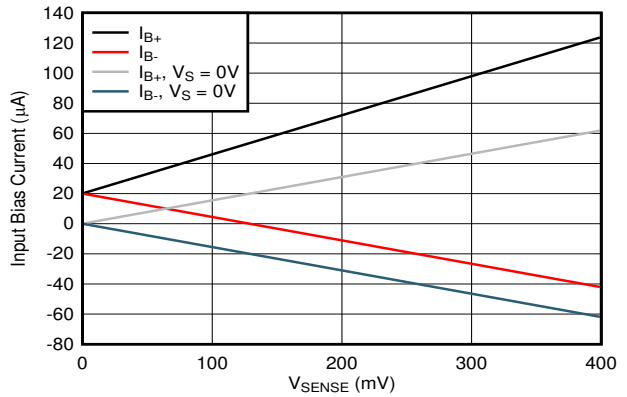


Figure 6-16. INA310x2-Q1, INA310x3-Q1 Input Bias Current vs VSENSE

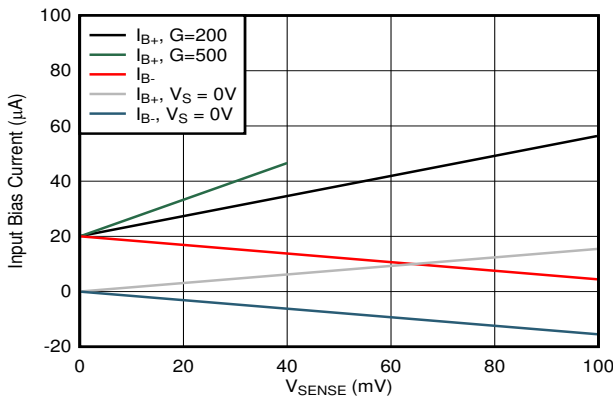


Figure 6-17. INA310x4-Q1, INA310x5-Q1 Input Bias Current vs VSENSE

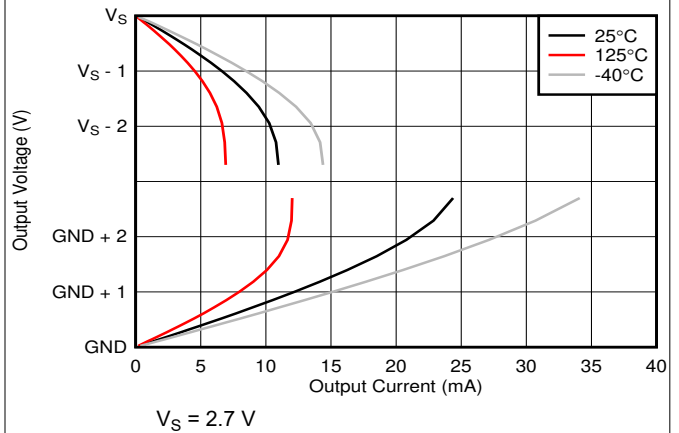


Figure 6-18. Output Voltage vs Output Current

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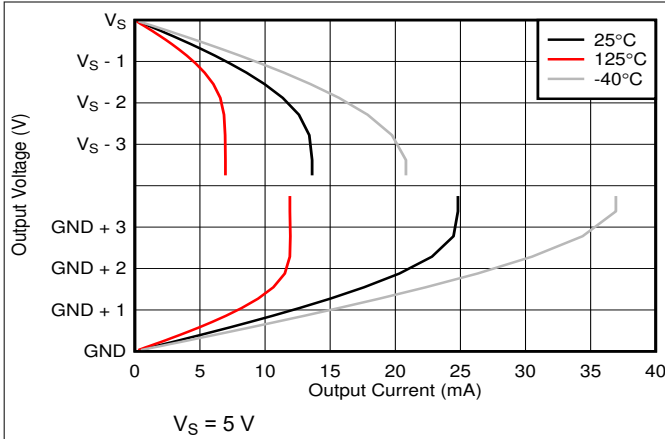


Figure 6-19. Output Voltage vs Output Current

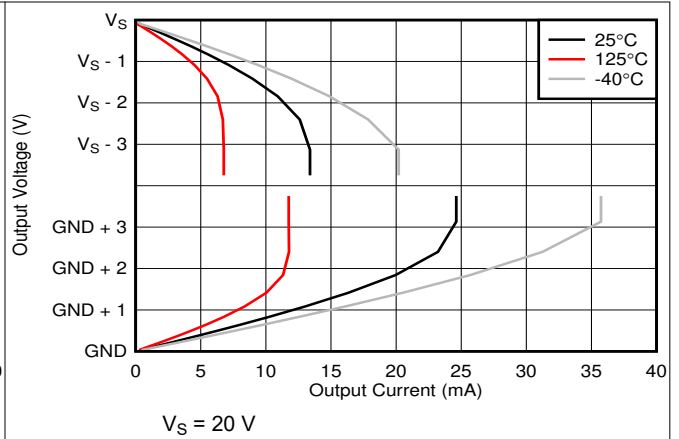


Figure 6-20. Output Voltage vs Output Current

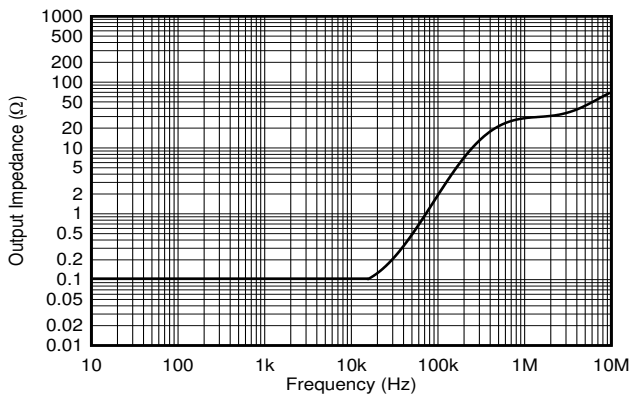


Figure 6-21. Output Impedance vs Frequency

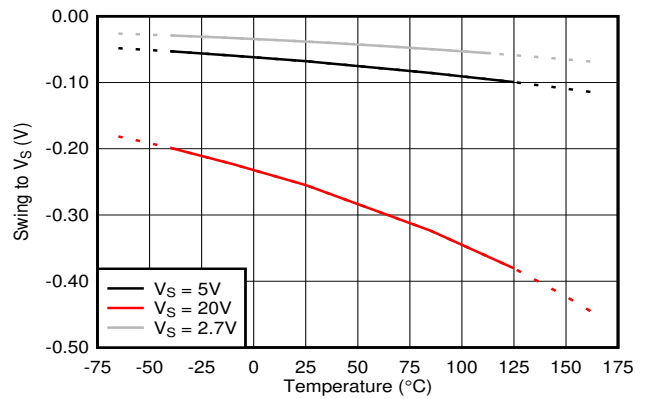


Figure 6-22. Swing to Supply vs Temperature

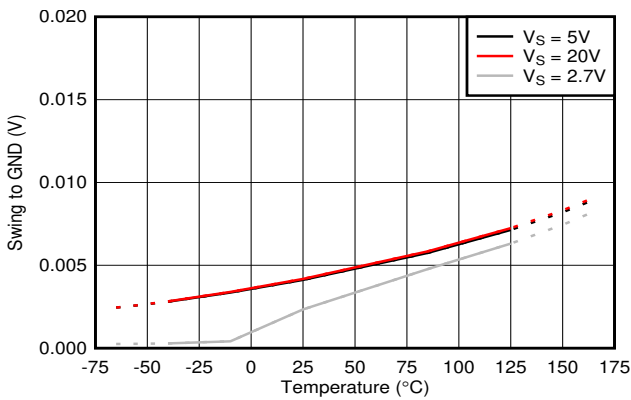


Figure 6-23. Swing to GND vs Temperature

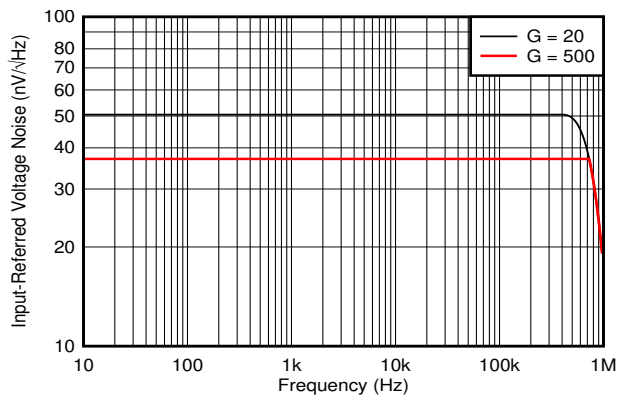


Figure 6-24. Input Referred Noise vs Frequency

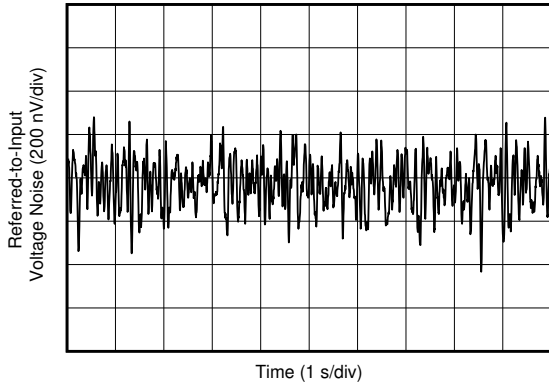


Figure 6-25. Input Referred Noise

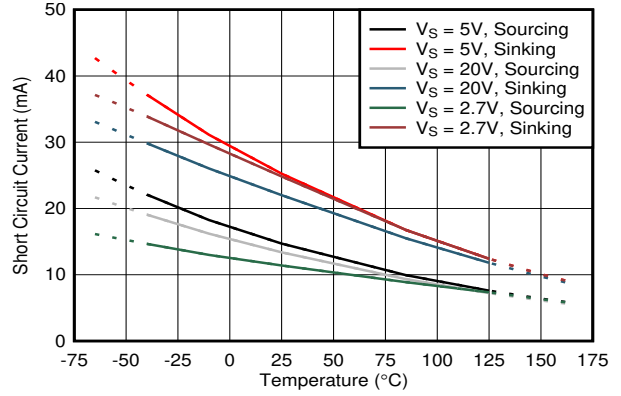


Figure 6-26. Short-Circuit Current vs Temperature

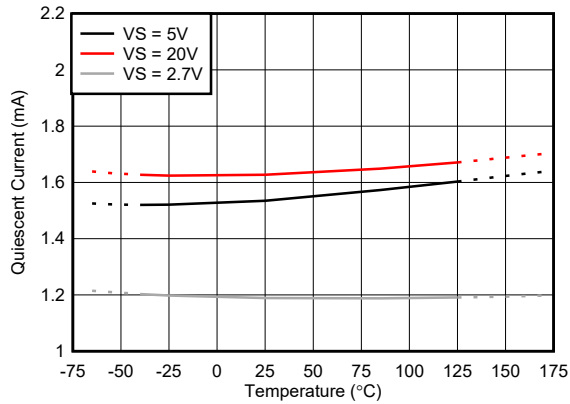


Figure 6-27. Quiescent Current vs Temperature

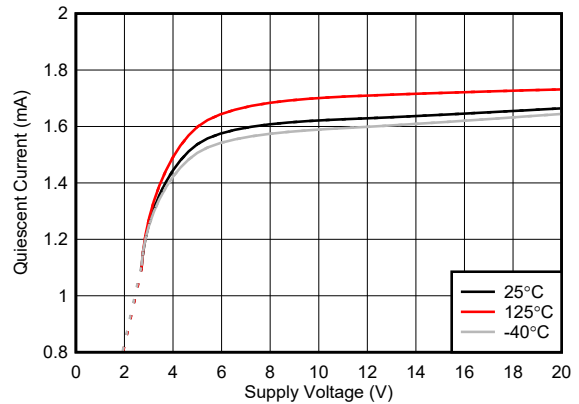


Figure 6-28. Quiescent Current vs Supply Voltage

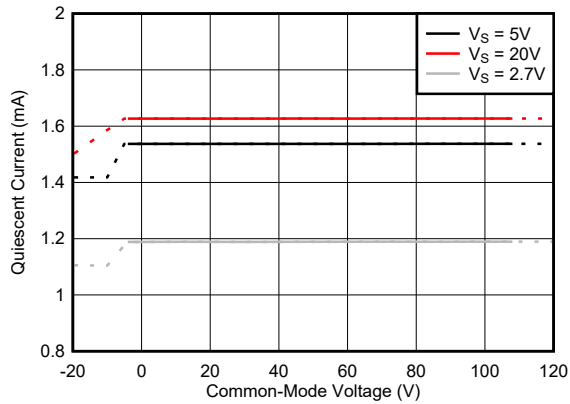


Figure 6-29. Quiescent Current vs Common-Mode Voltage

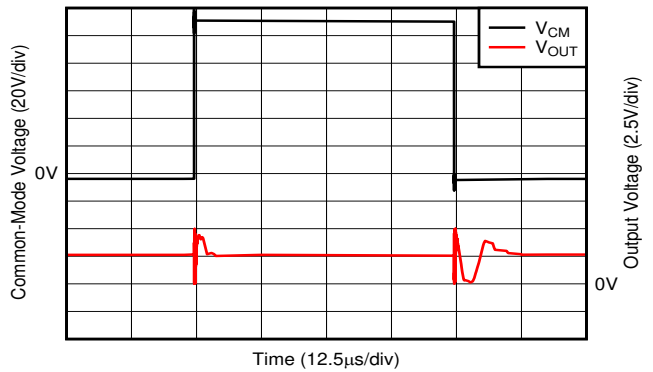


Figure 6-30. Common-Mode Voltage Fast Transient Pulse

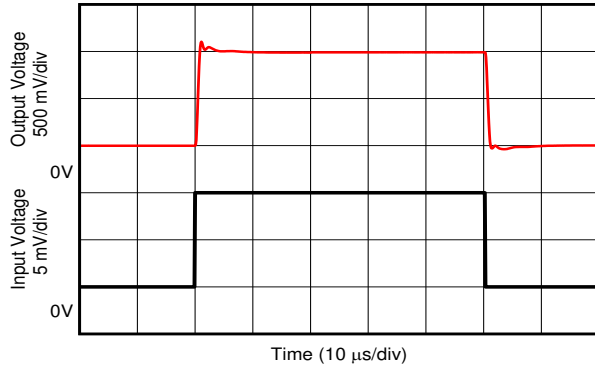


Figure 6-31. INA310x3-Q1 Step Response

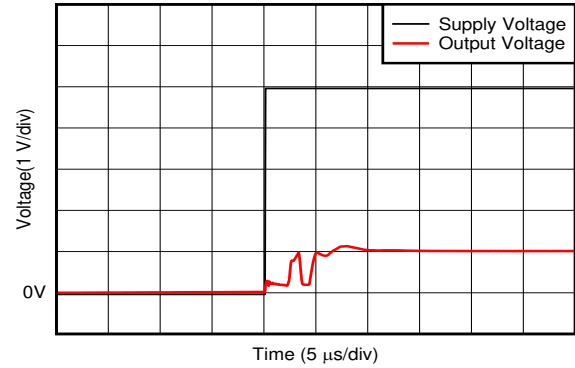


Figure 6-32. Start-Up Response

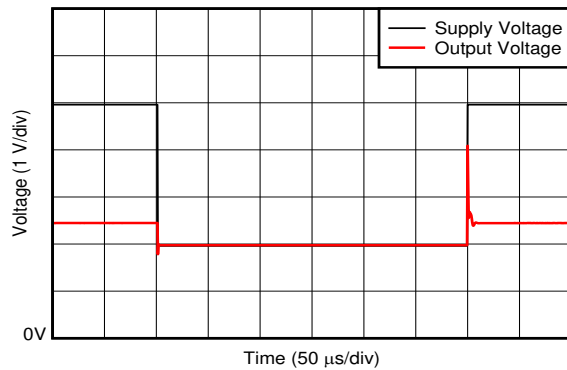


Figure 6-33. Supply Transient Response

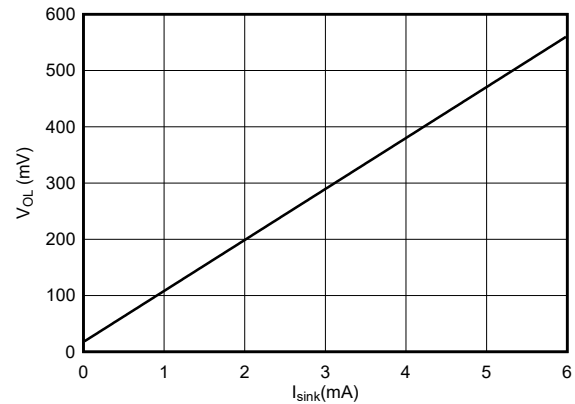


Figure 6-34. Comparator V_{OL} vs I_{SINK}

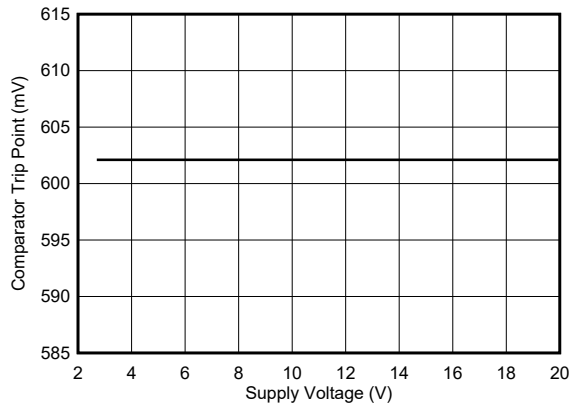


Figure 6-35. Comparator Trip Point vs Supply Voltage

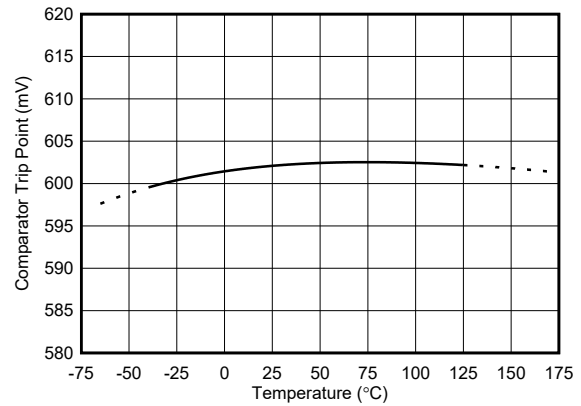


Figure 6-36. Comparator Trip Point vs Temperature

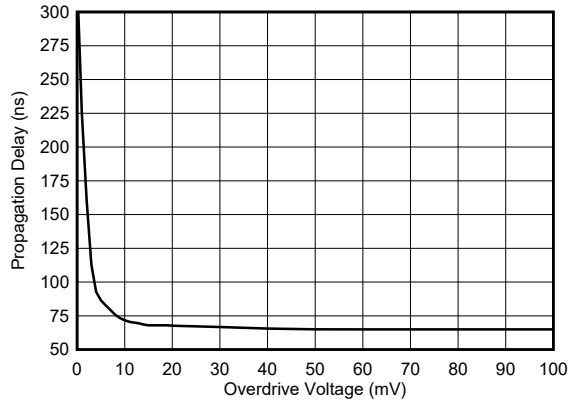


Figure 6-37. Comparator Propagation Delay vs Overdrive Voltage

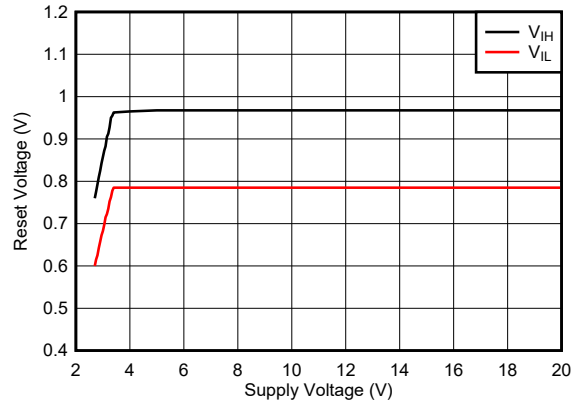


Figure 6-38. Comparator Reset Voltage vs Supply Voltage

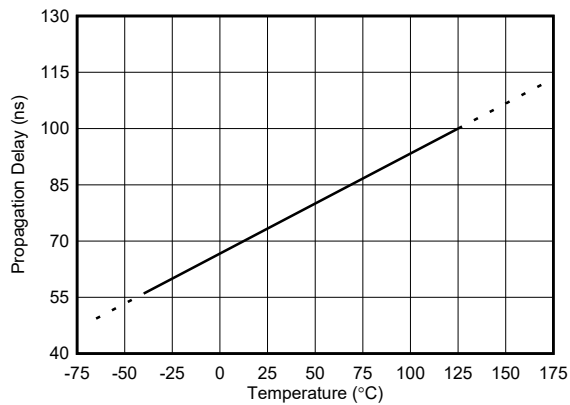


Figure 6-39. Comparator Propagation Delay vs Temperature

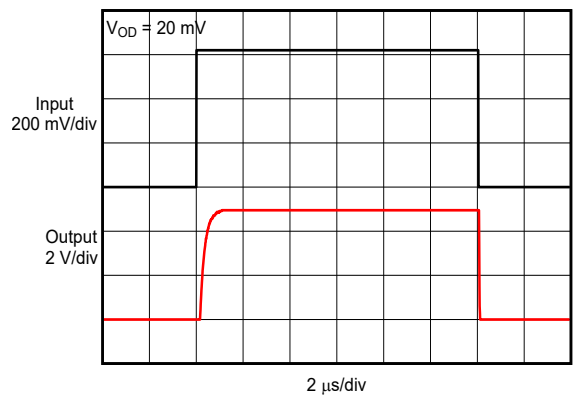


Figure 6-40. Comparator Propagation Delay

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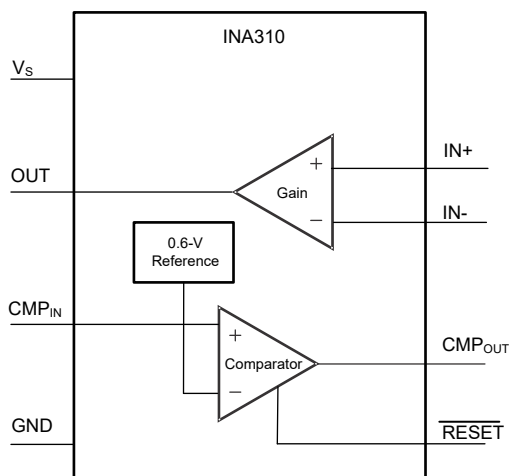
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7 Detailed Description

7.1 Overview

The INA310x-Q1 is a high or low-side high-speed current-sense amplifier that offers a wide common-mode range, precision zero-drift topology, excellent common-mode rejection ratio (CMRR) and fast slew rate. Different gain versions are available to optimize the output dynamic range based on the application. The INA310x-Q1 is designed using an architecture that enables low input bias current of 20 μ A with a specified common-mode voltage range from -4 V to 110 V with signal bandwidths up to 1.3 MHz. The INA310x-Q1 incorporates an open-drain comparator and internal reference providing a 0.6-V threshold. An external resistor divider sets the current trip point. The comparator includes a latching capability, that can be made transparent by grounding (or leaving open) the $\overline{\text{RESET}}$ pin (see the [RESET Function](#) section).

7.2 Functional Block Diagram



7.3 Feature Description

7.3.1 Amplifier Input Common-Mode Signal

The INA310x-Q1 supports large input common-mode voltages from -4 V to $+110$ V. The internal topology of the INA310x-Q1 enables the common-mode range to not be restricted by the power-supply voltage (V_S). Due to this feature, the INA310x-Q1 can be used for both low-side and high-side current-sensing applications that extend beyond the supply range of 2.7 V to 20 V.

7.3.2 Input-Signal Bandwidth

The INA310x-Q1 is available with several gain options, including 20 V/V, 50 V/V, 100 V/V, 200 V/V, and 500 V/V. The unique multistage design enables the amplifier to achieve high bandwidth at all gains. This high bandwidth provides the throughput and fast response that is required for the rapid detection and processing of overcurrent events.

7.3.3 Low Input Bias Current

The INA310x-Q1 inputs draw a 20- μ A input bias current per pin at a common-mode voltage as high as 110 V, which enables precision current sensing on applications that require lower current leakage. Unlike many high voltage current sense amplifiers whose input bias currents are proportional to the common-mode voltage, the input bias current of the INA310x-Q1 remains flat over the entire common-mode voltage range.

7.3.4 Low V_{SENSE} Operation

The INA310x-Q1 features high performance operation across the entire valid V_{SENSE} range. The zero-drift input architecture of the INA310x-Q1 provides the low offset voltage and low offset drift needed to measure low V_{SENSE} levels accurately across the wide operating temperature of -40°C to $+125^\circ\text{C}$. Low V_{SENSE} operation is particularly beneficial when using low ohmic shunts for high current measurements, as power losses across the

shunt are significantly reduced. V_{SENSE} low level is only limited by the output swing to GND (V_{SN}). The minimum V_{SENSE} is limited to V_{SN} divided by Gain.

7.3.5 Wide Fixed Gain Output

The INA310x-Q1 maximum gain error is 0.15% at room temperature, with a maximum drift of 10 ppm/°C over the full temperature range of -40°C to $+125^{\circ}\text{C}$. The INA310x-Q1 is available in multiple gain options of 20 V/V, 50 V/V, 100 V/V, 200 V/V, and 500 V/V, which the system designer should select based on their desired signal-to-noise ratio and other system requirements, such as the dynamic current range and full-scale output voltage target.

The INA310x-Q1 closed-loop gain is set by a precision, low-drift internal resistor network. The ratio of these resistors are excellently matched, while the absolute values may vary significantly. TI does not recommend adding additional resistance around the INA310x-Q1 to change the effective gain because of this variation.

7.3.6 Wide Supply Range

The INA310x-Q1 operates with a wide supply range from 2.7 V to 20 V. While the input voltage range of the INA310x-Q1 is independent of the supply voltage, the output voltage is bound by the supply voltage applied to the device. The output voltage can range from as low as 20 mV to as high as 200 mV below the supply voltage.

7.3.7 Integrated Comparator

The INA310x-Q1 incorporates an open-drain comparator with an internal reference providing a 0.6-V threshold. The comparator input (CMP_{IN}) can take voltage from 0 V up to 5.5 V or equal to power-supply voltage (if it is lower than 5.5 V). The comparator has a built-in hysteresis of 8 mV (typical). Figure 7-1 shows the hysteresis, which is the difference between the rising-edge threshold and the falling-edge threshold. The hysteresis makes stable switching at the comparator output by providing noise immunity at comparator input.

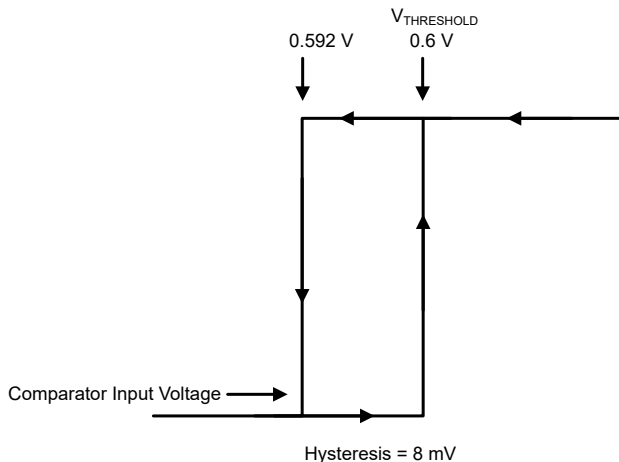


Figure 7-1. The Comparator Threshold and Hysteresis

The open-drain output of the comparator can be tied to voltage range of 0 to 20 V (independent of power supply) through a pullup resistor. When the voltage at the comparator input (CMP_{IN}) exceeds 0.6 V, the output of the comparator goes high. When the voltage at the comparator input falls below falling-threshold ($0.6\text{ V} - \text{Hysteresis}$), the output of the comparator is pulled low by an internal open-drain transistor.

7.3.8 RESET Function

The $\overline{\text{RESET}}$ function allows the comparator to work in transparent mode or latching mode. Figure 7-2 shows the two modes of the RESET function. When the RESET pin is left open or connected to GND the comparator functions in a transparent mode. In transparent mode comparator output (CMP_{OUT}) responds as a normal comparator. When the $\overline{\text{RESET}}$ pin is connected to the supply voltage, the pin operates in latching mode. In the latching mode when the comparator is triggered by the comparator input going higher than 0.6 V, the output of the comparator stays high irrespective of comparator input after. To release the comparator from the latching

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mode, the $\overline{\text{RESET}}$ pin must be pulled to GND or released to open. The $\overline{\text{RESET}}$ pin can take a voltage range from 0 V to the power-supply voltage.

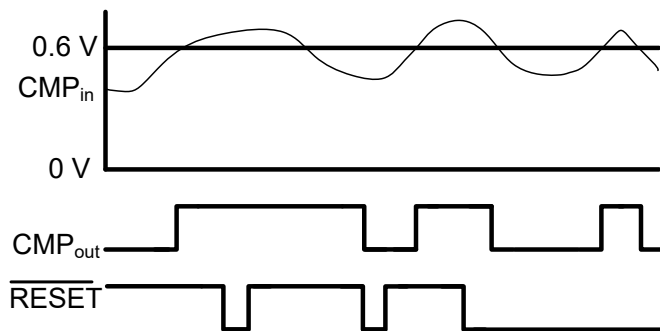


Figure 7-2. The Comparator $\overline{\text{RESET}}$ Function

7.3.9 Short Propagation Delay

The combination of a high-speed current sense amplifier and a fast comparator provides a short total propagation delay of 1 μs . The sense voltage (across the shunt resistor) propagates through the output where the output is divided down with the resistor divider to the comparator input and then to the comparator output. An external resistor divider at V_{OUT} sets overcurrent threshold. The total propagation delay is time taken from when the sense voltage (across the shunt resistor) exceeds the overcurrent threshold to when the comparator output drives high. The short propagation delay makes the INA310x-Q1 well suited for overcurrent protection in systems sensitive to overcurrent events.

7.3.10 Comparator Input Bias Current

The INA310x-Q1 comparator input has a built-in circuit to protect the input devices in case of large input differential voltage. This circuit results in the input bias current (I_{BCMPIN}) curve against input voltage (V_{CMPIN}) as shown in [Figure 7-3](#). The I_{BCMPIN} reduces with V_{CMPIN} from 0 V to 0.4 V, I_{BCMPIN} is under 20 nA at 25°C for V_{CMPIN} range from 0.4 V to 1.2 V, and I_{BCMPIN} increases with V_{CMPIN} from 1.8 V to 5.5 V. The nature of I_{BCMPIN} does not contribute to the inaccuracy of the comparator alert threshold voltage ($V_{\text{THRESHOLD}}$) significantly because the I_{BCMPIN} goes below 20 nA when the input voltage is close to the threshold voltage (0.6 V). Avoid using a high-value resistor for the divider network for better $V_{\text{THRESHOLD}}$ accuracy. The sum of the two resistors in the divider network as shown in [Overcurrent Threshold Connection](#) is recommended to keep lower than 100 k Ω .

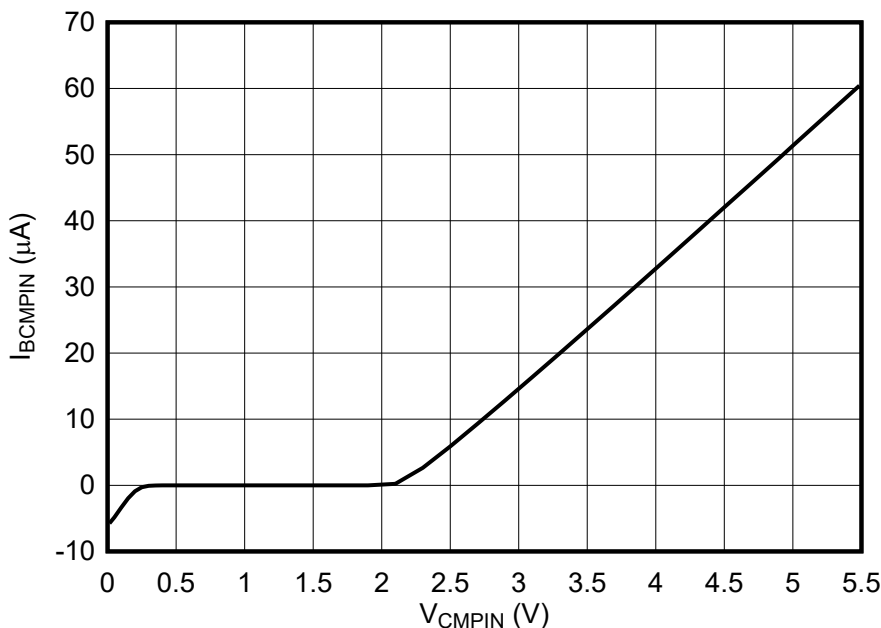


Figure 7-3. Comparator I_{BCMPIN} vs V_{CMPIN}

7.4 Device Functional Modes

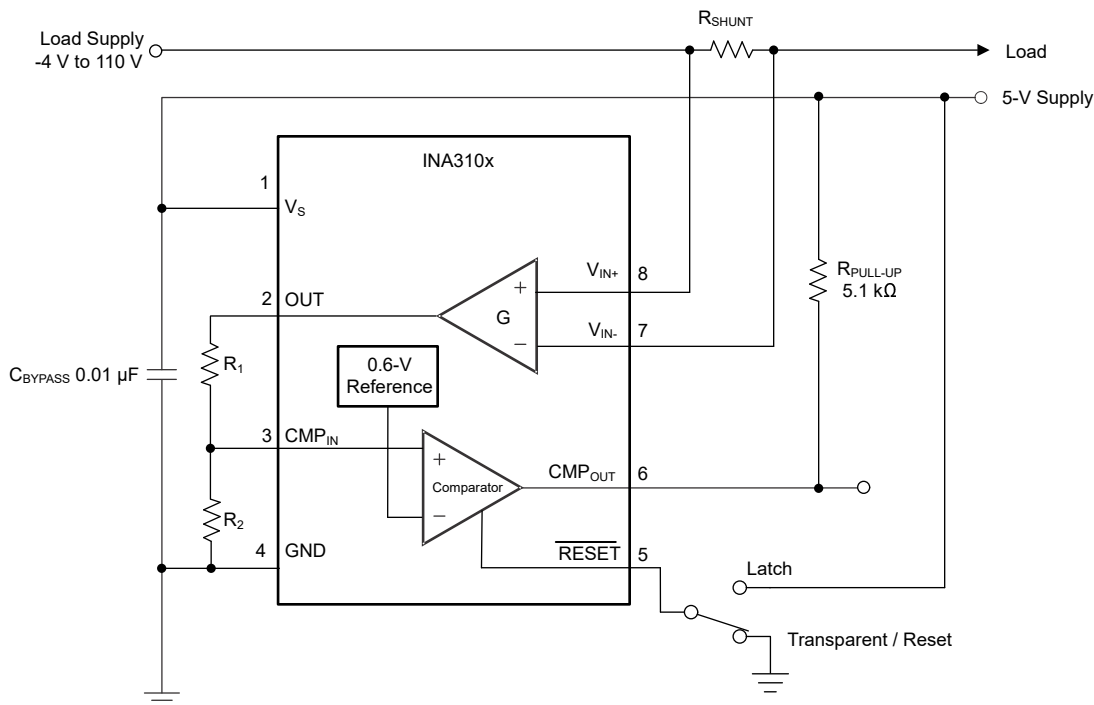
7.4.1 Basic Connections

Figure 7-4 shows a basic circuit connection for INA310x-Q1. The INA310x-Q1 is configurable to allow for unidirectional high-side or low-side, current-sensing operation. The input pins (IN+ and IN-) must be connected as closely as possible with Kelvin connections to the shunt resistor to minimize any resistance in series with the shunt resistance. The [Layout](#) section provides the layout guidelines and a layout example.

Power-supply bypass capacitors are required for stability. Applications with noisy or high-impedance power supplies may require additional decoupling capacitors to reject power-supply noise. Connect bypass capacitors close to the device V_S pin. The recommended value of a bypass capacitor is 0.01 μF .

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**Figure 7-4. INA310x-Q1 Basic Connections****7.4.1.1 Overcurrent Threshold Connection**

The INA310x-Q1 comparator in [Figure 7-4](#) is configured to provide overcurrent alert signal when the current through R_{SHUNT} exceeds the overcurrent threshold. OUT voltage times R_2 divided by R_1 and R_2 compared to the internal reference voltage (0.6 V) sets the overcurrent threshold. [Equation 1](#) shows the relation of the overcurrent threshold with gain, R_{SHUNT} , R_1 and R_2 .

$$I_{Sense_Alert_Threshold} = \frac{0.6 \times (R_1 + R_2)}{R_2 \times G \times R_{shunt}} \quad (1)$$

R_1 and R_2 load OUT, therefore TI recommends to set the sum of these resistors higher than 10k. This helps keep the high swing range at the OUT and lower total supply current. The high value of these resistors will contribute to inaccuracy in comparator alert threshold voltage ($V_{THRESHOLD}$) as mentioned in [Comparator Input Bias Current](#). The [Design Requirements](#) section shows an example of resistors values to set the overcurrent threshold.

7.4.2 High-Side Switch Overcurrent Shutdown

The INA310x-Q1 measures differential voltage developed by current flowing through a current-shunt resistor. Figure 7-5 shows the circuit with INA310x-Q1 used for turning off the high-side switch in case of overcurrent. When the current exceeds overcurrent threshold, the comparator output (CMP_{OUT}) signal goes high. This signal from the comparator drives through the Q1 transistor to the gate of the high-side switch, causing the switch to shut down. The Q1 transistor helps isolate CMP_{OUT} from the high voltage of the Supply. There are three location options to have shunt resistor to measure unidirectional current. Option 1 and Option 2 are high-side current sensing, and Option 3 is low-side current sensing. Though both are high-side current sensing, Option 1 accounts for the current flowing through the Q1 transistor, and Option 2 does not. The advantages of high-side current sensing are that high-side sensing options do not contribute to ground disturbances and that high-side sensing can detect load shorts. In high-side current sensing, input common-mode is close to the power supply so a current-sensing amplifier with high CMRR and high common-mode is required for high-accuracy measurement. The low-side current sensing does not require a high-voltage, current-sensing amplifier as common mode remains very close to the ground. The disadvantages of low-side current sensing are that low-side sensing options contribute to ground disturbances and that low-side current sensing cannot detect load shorts.

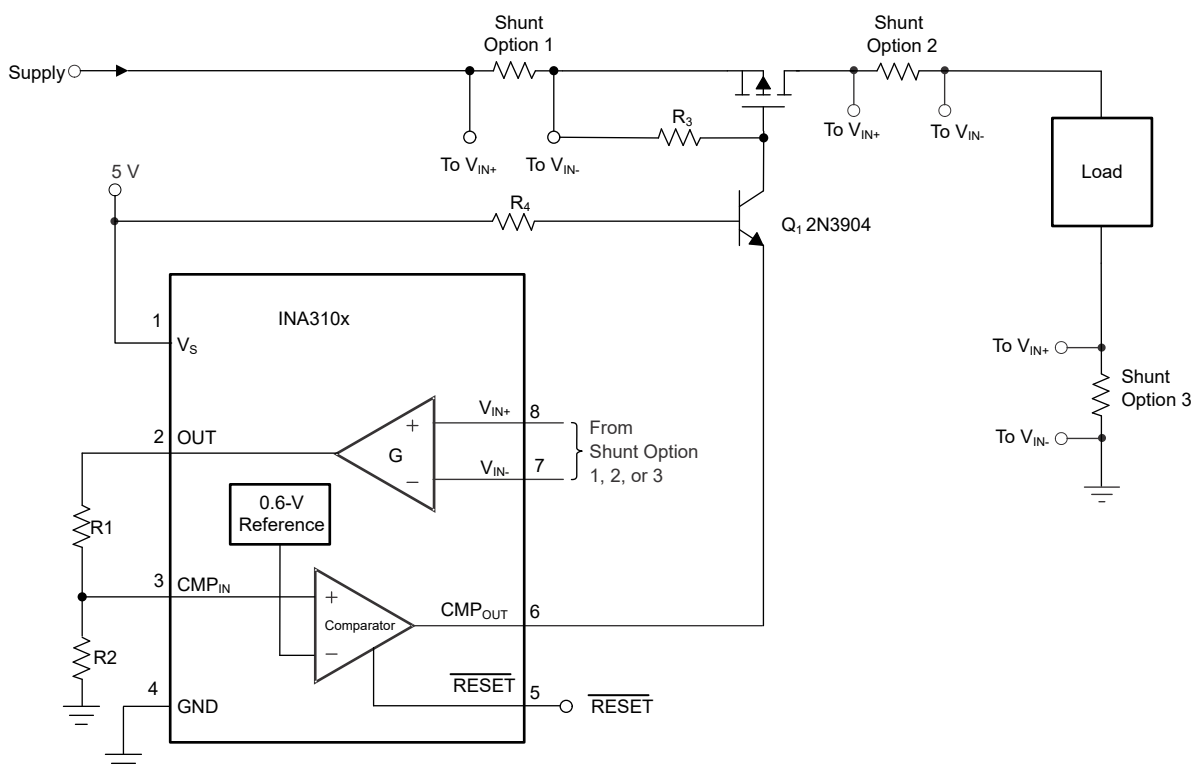


Figure 7-5. High-Side Switch for Overcurrent Shutdown

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7.4.3 Bidirectional Overcurrent Comparator

The INA310x-Q1 can operate only in unidirectional mode, but [Figure 7-6](#) shows that two INA310x-Q1s can be configured to provide a bidirectional overcurrent alert signal. The polarity of the differential voltage measured across the shunt resistor is in reverse for one current sense amplifier. Two INA310x-Q1 function to cover the opposite current directions, and therefore provide bidirectional overcurrent monitor function.

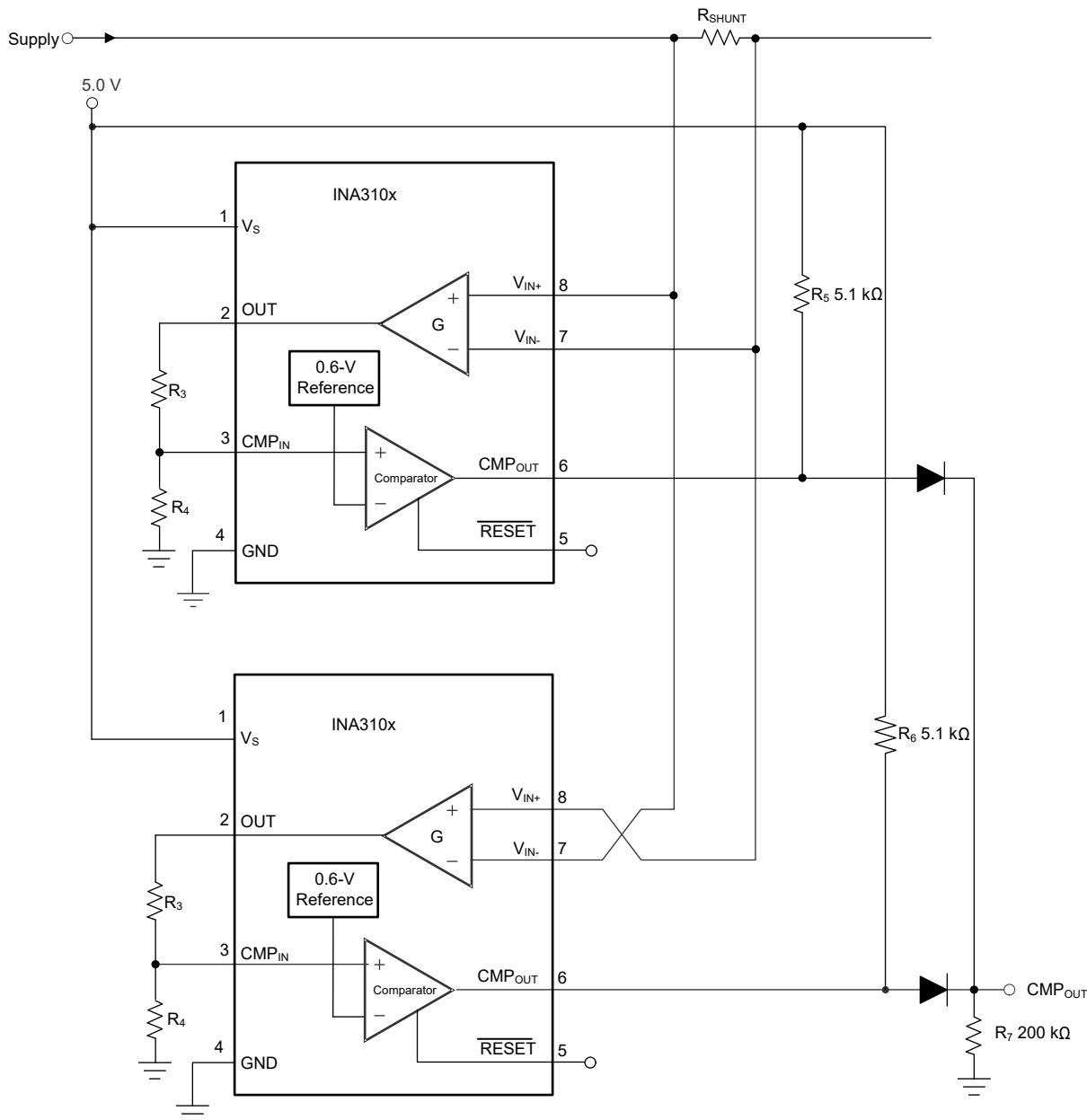


Figure 7-6. Ground Referenced Output

8 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

8.1 Application Information

The INA310x-Q1 amplifies the voltage developed across a current-sensing resistor as current flows through the resistor to the load. The wide input common-mode voltage range and high common-mode rejection of the INA310x-Q1 make the device usable over a wide range of voltage rails while still maintaining accurate current measurement.

8.1.1 R_{SENSE} and Device Gain Selection

To maximize the accuracy of a current sense amplifier, TI recommends to choose the largest current sense resistor value possible in an application. A larger value sense resistor maximizes the differential input signal for a given amount of current flow and reduces the error contribution of the offset voltage. However, there are practical limits as to how large the current-sense resistor value can be in a given application because of the physical dimensions of the resistor, package construction and maximum power dissipation. [Equation 2](#) gives the maximum value for the current-sense resistor for a given power dissipation budget:

$$R_{\text{SENSE}} < \frac{PD_{\text{MAX}}}{I_{\text{MAX}}^2} \quad (2)$$

where:

- PD_{MAX} is the maximum allowable power dissipation in R_{SENSE} .
- I_{MAX} is the maximum current that will flow through R_{SENSE} .

An additional limitation on the size of the current sense resistor and device gain is due to the power-supply voltage, V_S , and device swing-to-rail limitations. To make sure that the current-sense signal is properly passed to the output, both positive and negative output swing limitations must be examined. [Equation 3](#) provides the maximum values of R_{SENSE} and GAIN to keep the device from exceeding the positive swing limitation.

$$I_{\text{MAX}} \times R_{\text{SENSE}} \times \text{GAIN} < V_{\text{SP}} \quad (3)$$

where:

- I_{MAX} is the maximum current that will flow through R_{SENSE} .
- GAIN is the gain of the current-sense amplifier.
- V_{SP} is the positive output swing as specified in the data sheet.

To avoid positive output swing limitations when selecting the value of R_{SENSE} , there is always a trade-off between the value of the sense resistor and the gain of the device under consideration. If the sense resistor selected for the maximum power dissipation is too large, then it is possible to select a lower-gain device to avoid positive swing limitations.

The negative swing limitation places a limit on how small the sense resistor value can be for a given application. [Equation 4](#) provides the limit on the minimum value of the sense resistor.

$$I_{\text{MIN}} \times R_{\text{SENSE}} \times \text{GAIN} > V_{\text{SN}} \quad (4)$$

where:

- I_{MIN} is the minimum current that will flow through R_{SENSE} .

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- GAIN is the gain of the current-sense amplifier.
- V_{SN} is the negative output swing of the device.

Table 8-1 shows an example of the different results obtained from using five different gain versions of the INA310x-Q1. From the table data, the highest gain device allows a smaller current-shunt resistor and decreased power dissipation in the element.

Table 8-1. R_{SENSE} Selection and Power Dissipation⁽¹⁾

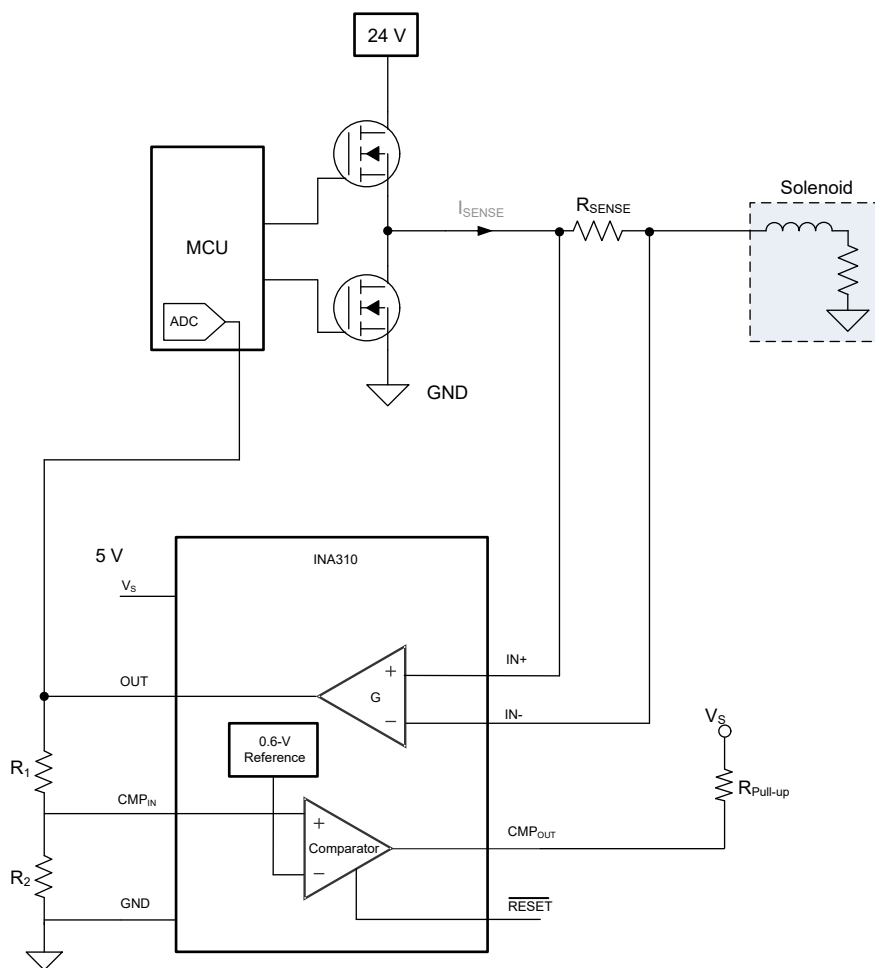
| PARAMETER | | EQUATION | RESULTS AT $V_S = 5\text{ V}$ | | | | |
|-------------|--|----------------------------------|-------------------------------|----------------|----------------|----------------|----------------|
| | | | A1, B1 DEVICES | A2, B2 DEVICES | A3, B3 DEVICES | A4, B4 DEVICES | A5, B5 DEVICES |
| G | Gain | | 20 V/V | 50 V/V | 100 V/V | 200 V/V | 500 V/V |
| V_{DIFF} | Ideal differential input voltage | $V_{DIFF} = V_{OUT} / G$ | 250 mV | 100 mV | 50 mV | 25 mV | 10mV |
| R_{SENSE} | Current sense resistor value | $R_{SENSE} = V_{DIFF} / I_{MAX}$ | 25 m Ω | 10 m Ω | 5 m Ω | 2.5 m Ω | 1 m Ω |
| P_{SENSE} | Current-sense resistor power dissipation | $R_{SENSE} \times I_{MAX}^2$ | 2.5 W | 1 W | 0.5 W | 0.25 W | 0.1 W |

(1) Design example with 10-A full-scale current with maximum output voltage set to 5 V.

8.2 Typical Application

The INA310x-Q1 is a unidirectional, current-sense amplifier capable of measuring currents through a resistive shunt with shunt common-mode voltages from -4 V to $+110\text{ V}$.

8.2.1 Current Sensing in a Solenoid Application


Figure 8-1. Current Sensing in a Solenoid Application

8.2.1.1 Design Requirements

In this example application, the common-mode voltage ranges from 0 V to 24 V. The maximum sense current is 1.5 A, an alert must be indicated if the current exceeds 1.9 A, and a 5 V supply is available for the INA310x-Q1. Following the design guidelines from [R_{SENSE} and Device Gain Selection](#), a R_{SENSE} of 50 mΩ and a gain of 50 V/V are selected to provide good output dynamic range. [Table 8-2](#) lists the design setup for this application.

Table 8-2. Design Parameters

| DESIGN PARAMETERS | EXAMPLE VALUE |
|-----------------------------|---------------|
| Power supply voltage | 5 V |
| Common mode voltage range | 0 V to 24 V |
| Maximum sense current | 1.5 A |
| R _{SENSE} resistor | 50 mΩ |
| Gain option | 50 V/V |
| Over-current Threshold | 1.9 A |
| R ₁ | 69.15 kΩ |
| R ₂ | 10 kΩ |

8.2.1.2 Detailed Design Procedure

The INA310x-Q1 is designed to measure current in a typical solenoid application. The INA310x-Q1 measures current across the 50-mΩ shunt that is placed at the output of the half-bridge. The INA310x-Q1 measures the differential voltage across the shunt resistor, and the signal is internally amplified with a gain of 50 V/V. The output of the INA310x-Q1 is connected to the analog-to-digital converter (ADC) of an MCU to digitize the current measurements.

R₂ is fixed as 10 kΩ to avoid loading of OUT as recommended in [Overcurrent Threshold Connection](#). R₁ is calculated as 69.15 kΩ using [Equation 1](#).

$$1.9 \text{ A} = \frac{0.6 \text{ V} \times (R_1 + 10 \text{ k}\Omega)}{10 \text{ k}\Omega \times 50 \times 50 \text{ m}\Omega}$$

R₁ (69.15 kΩ) and R₂ (10 kΩ) divides down the output which is an input to the comparator. This sets the overcurrent alert threshold of 1.9 A.

Solenoid loads are highly inductive and are often prone to failure. Solenoids are often used for position control, precise fluid control, and fluid regulation. Measuring real-time current on the solenoid continuously can indicate premature failure of the solenoid, which can lead to a faulty control loop in the system. Measuring high-side current also indicates if there are any ground faults on the solenoid or the FETs that can be damaged in an application. The INA310x-Q1, with high bandwidth and slew rate, can be used to detect fast overcurrent conditions to prevent the solenoid damage from short-to-ground faults.

8.2.1.3 Overload Recovery With Negative V_{SENSE}

The INA310x-Q1 is a unidirectional current sense amplifier that is meant to operate with a positive differential input voltage (V_{SENSE}). If negative V_{SENSE} is applied, the device is placed in an overload or saturated condition and requires time to recover after V_{SENSE} returns positive. The required overload recovery time increases with more negative V_{SENSE}.

8.2.1.4 Application Curve

Figure 8-2 shows the output response of a solenoid.

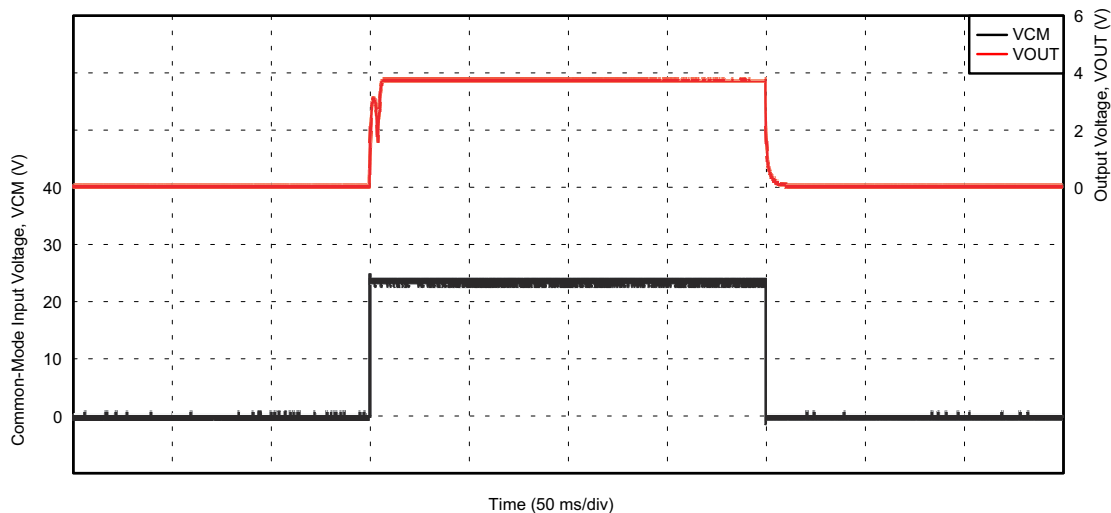


Figure 8-2. Solenoid Control Current Response

8.2.2 Low-Side Switch Overcurrent Shutdown

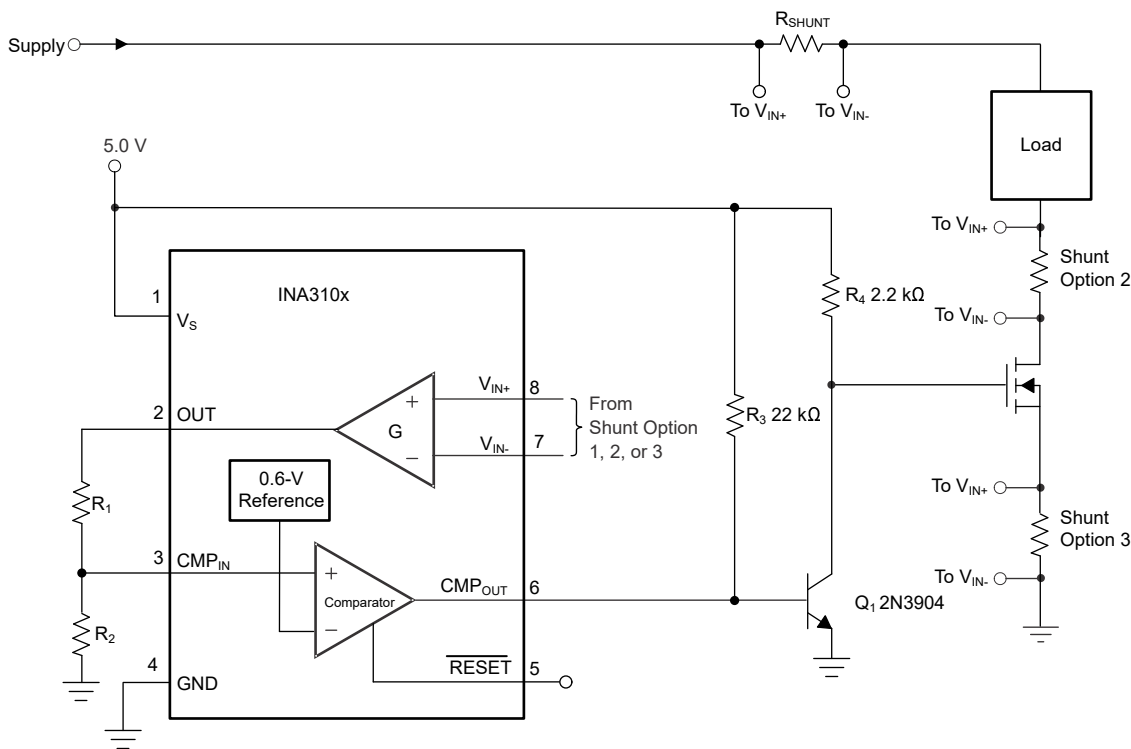


Figure 8-3. Low-Side Switch Overcurrent Shutdown

8.2.2.1 Design Requirements

The INA310x-Q1 measures current through a resistive shunt with current flowing in one direction that enables detection of an overcurrent event only when the differential input voltage exceeds the threshold limit. When the current reaches the set limit of the divider of R_1 and R_2 , the output of comparator (CMP_{OUT}) transitions high, which turns on Q_1 , pulls the gate of the pass-FET low, and turns off the flow of the current. In this example application, the common-mode voltage is set at 5 V. The maximum sense current is 1 A, an alert must be

indicated if the current exceeds 1.2 A, and a 5 V supply is available for the INA310x-Q1. Following the design guidelines from [R_{SENSE} and Device Gain Selection](#), a R_{SHUNT} of 100 mΩ and a gain of 20 V/V are selected to provide a good output dynamic range. [Table 8-3](#) lists the design setup for this application.

Table 8-3. Design Parameters

| DESIGN PARAMETERS | EXAMPLE VALUE |
|-----------------------------|---------------|
| Power supply voltage | 5 V |
| Common mode voltage range | 5 V |
| Maximum sense current | 1 A |
| R _{SENSE} resistor | 100 mΩ |
| Gain option | 20 V/V |
| Over-current Threshold | 1.2 A |
| R ₁ | 10.2 kΩ |
| R ₂ | 3.4 kΩ |

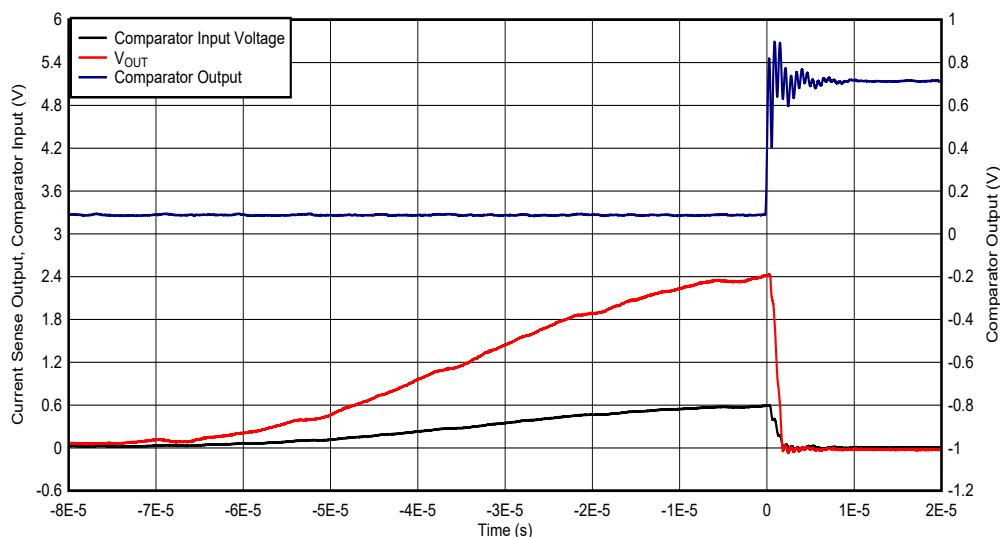
8.2.2.2 Detailed Design Procedure

[Figure 8-3](#) shows the basic connections to the INA310x-Q1. The inputs terminals (IN+ and IN–) must be connected to the current sense resistor as close as possible to minimize any resistance in series with the shunt resistor. The INA310x-Q1 measures current across the 100-mΩ shunt that is placed in series with load. The INA310x-Q1 measures the differential voltage across the shunt resistor, and the signal is internally amplified with a gain of 20 V/V.

R₁ is fixed as 10.2 kΩ to avoid loading of OUT as recommended in [Overcurrent Threshold Connection](#). R₂ is calculated as 3.4 kΩ using [Equation 1](#). R₁ (10.2 kΩ) and R₂ (3.4 kΩ) divides down the output which is an input to the comparator. This sets the overcurrent alert threshold of 1.2 A.

8.2.2.3 Application Curve

[Figure 8-4](#) shows the output response the current sense amplifier and the comparator in event of overcurrent.

**Figure 8-4. Low-Side Switch Overcurrent Shutdown Response**

8.3 Power Supply Recommendations

The INA310x-Q1 makes accurate measurements beyond the connected power-supply voltage (V_S) because the inputs (IN+ and IN–) can operate anywhere between –4 V and 110 V independent of V_S . For example, with the V_S power supply equal to 5 V, the common-mode voltage of the measured shunt can be as high as 110 V.

INA310A-Q1, INA310B-Q1

SBOSAD3 – MAY 2023

8.3.1 Power Supply Decoupling

Place the power-supply bypass capacitor as close to the power-supply and ground pins as possible. TI recommends a bypass capacitor value of 0.1 μF . Additional decoupling capacitance can be added to compensate for noisy or high-impedance power supplies.

8.4 Layout

8.4.1 Layout Guidelines

Attention to good layout practices is always recommended.

- Connect the input pins to the sensing resistor using a Kelvin or 4-wire connection. This connection technique makes sure that only the current-sensing resistor impedance is detected between the input pins. Poor routing of the current-sensing resistor commonly results in additional resistance present between the input pins. Given the very low ohmic value of the current resistor, any additional high-current carrying impedance can cause significant measurement errors.
- Place the power-supply bypass capacitor as close to the device power-supply and ground pins as possible. The recommended value of this bypass capacitor is 0.1 μF . Additional decoupling capacitance can be added to compensate for noisy or high-impedance power supplies.

8.4.2 Layout Example

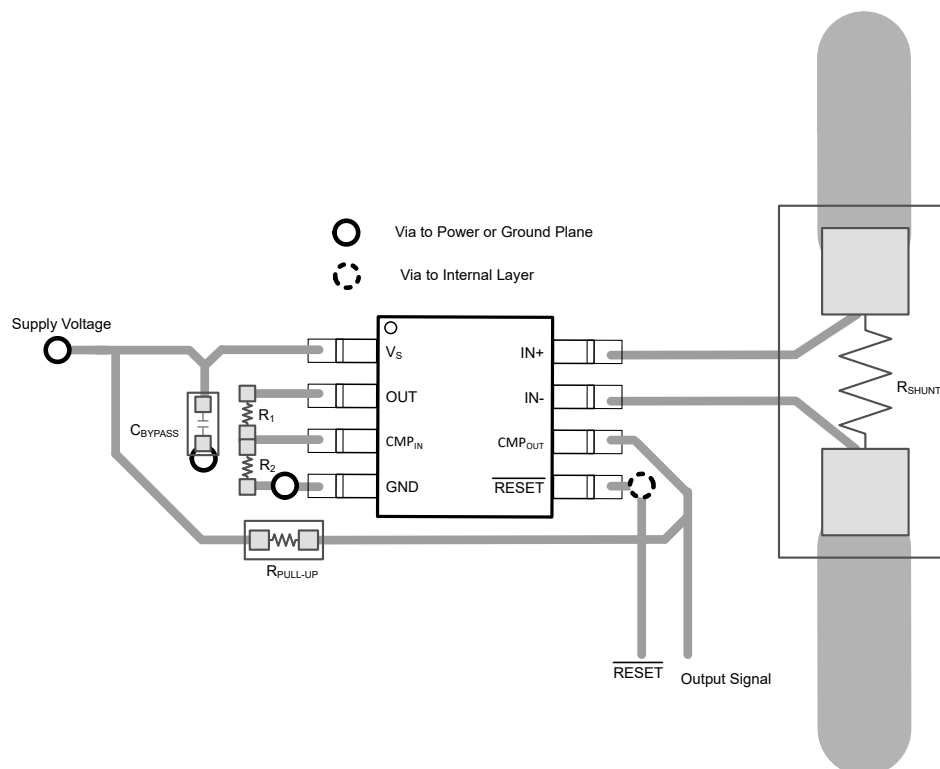


Figure 8-5. INA310x-Q1 Recommended Layout

9 Device and Documentation Support

9.1 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

9.2 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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9.3 Trademarks

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9.4 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

9.5 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

| Orderable Device | Status (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan (2) | Lead finish/ Ball material (6) | MSL Peak Temp (3) | Op Temp (°C) | Device Marking (4/5) | Samples |
|------------------|---------------|--------------|-----------------|------|-------------|-----------------|--------------------------------------|----------------------|--------------|-------------------------|-------------------------|
| INA310A1QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OQB | Samples |
| INA310A2QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OPB | Samples |
| INA310A3QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OQB | Samples |
| INA310A4QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2ORB | Samples |
| INA310A5QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OSB | Samples |
| INA310B1QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OTB | Samples |
| INA310B2QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OUB | Samples |
| INA310B3QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OVB | Samples |
| INA310B4QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OWB | Samples |
| INA310B5QDGKRQ1 | ACTIVE | VSSOP | DGK | 8 | 2500 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | 2OXB | Samples |

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

⁽⁵⁾ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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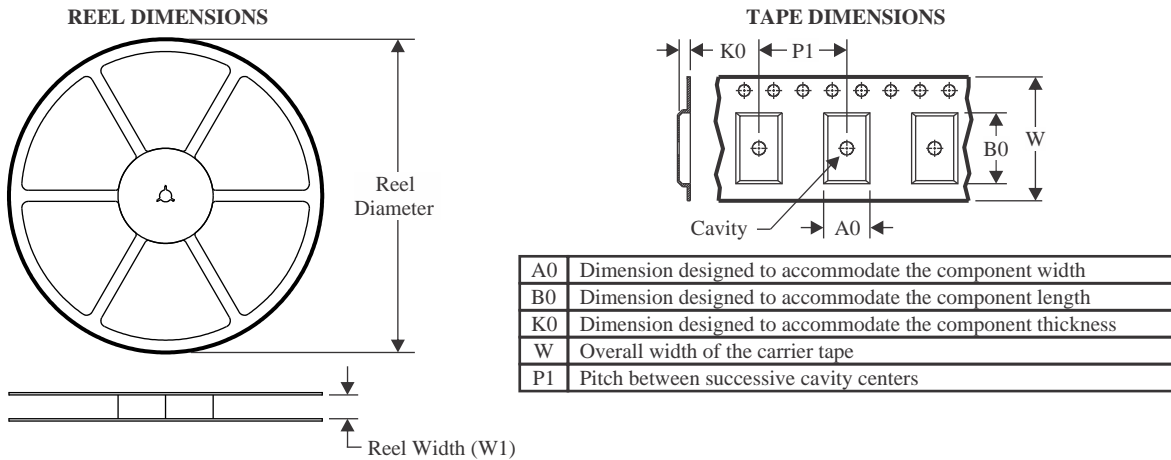
OTHER QUALIFIED VERSIONS OF INA310A-Q1, INA310B-Q1 :

- Catalog : [INA310A](#), [INA310B](#)

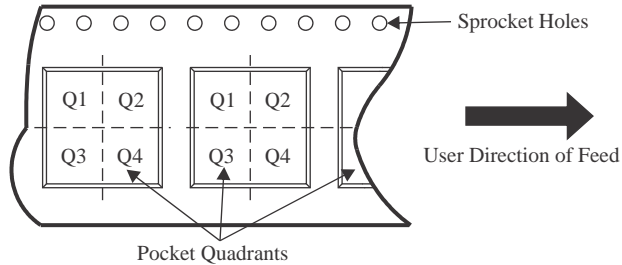
NOTE: Qualified Version Definitions:

- Catalog - TI's standard catalog product

TAPE AND REEL INFORMATION



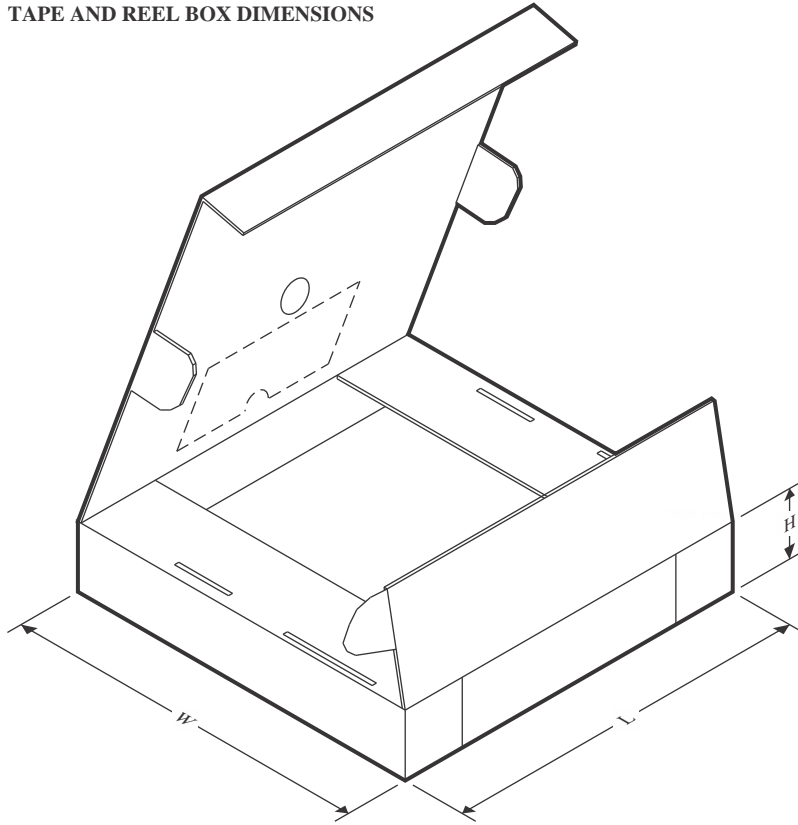
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

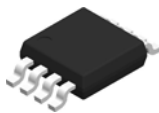
| Device | Package Type | Package Drawing | Pins | SPQ | Reel Diameter (mm) | Reel Width W1 (mm) | A0 (mm) | B0 (mm) | K0 (mm) | P1 (mm) | W (mm) | Pin1 Quadrant |
|-----------------|--------------|-----------------|------|------|--------------------|--------------------|---------|---------|---------|---------|--------|---------------|
| INA310A1QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310A2QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310A3QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310A4QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310A5QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310B1QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310B2QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310B3QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310B4QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| INA310B5QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
|-----------------|--------------|-----------------|------|------|-------------|------------|-------------|
| INA310A1QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310A2QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310A3QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310A4QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310A5QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310B1QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310B2QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310B3QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310B4QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |
| INA310B5QDGKRQ1 | VSSOP | DGK | 8 | 2500 | 356.0 | 356.0 | 35.0 |

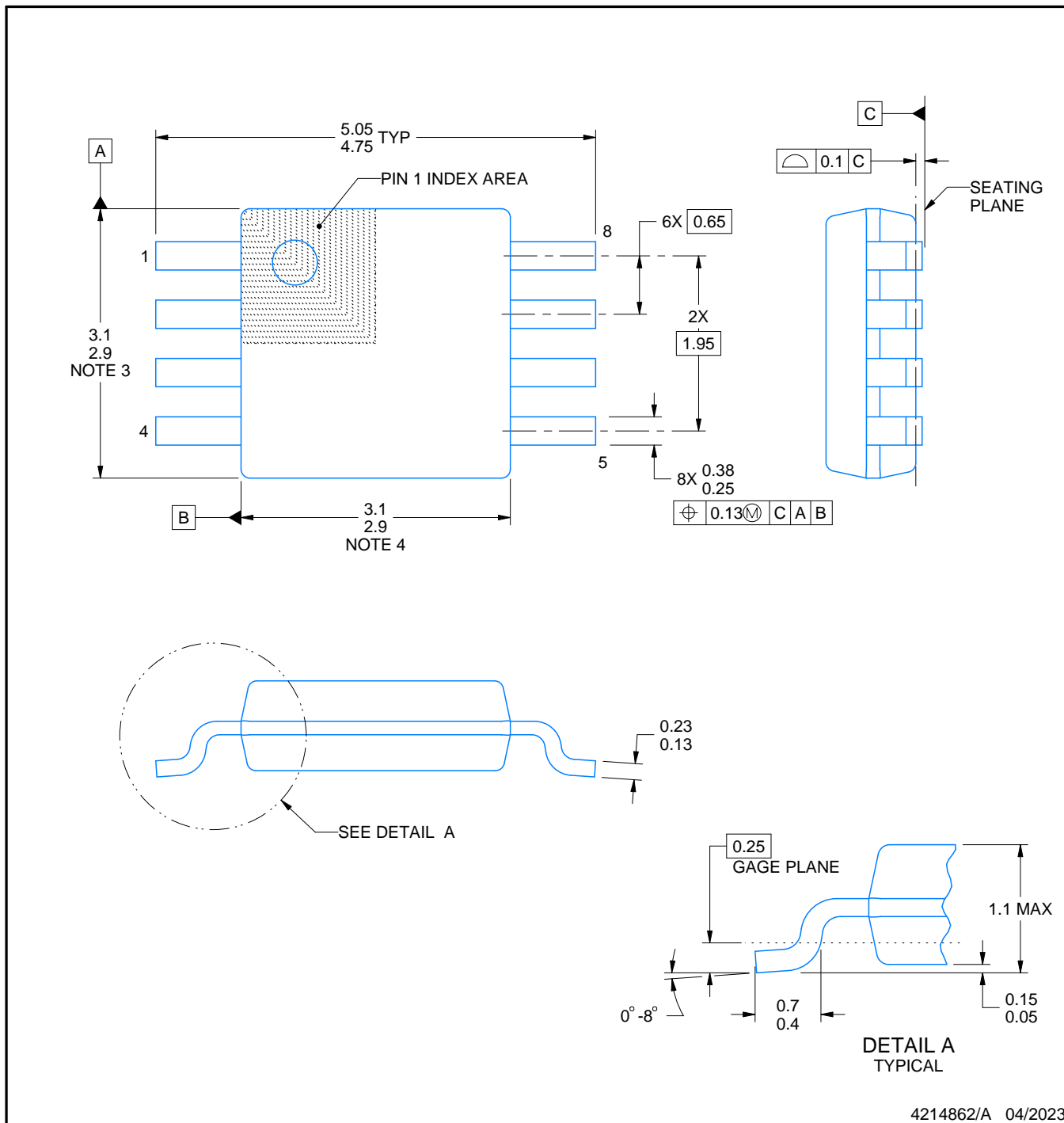


DGK0008A

PACKAGE OUTLINE

VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



4214862/A 04/2023

NOTES:

PowerPAD is a trademark of Texas Instruments.

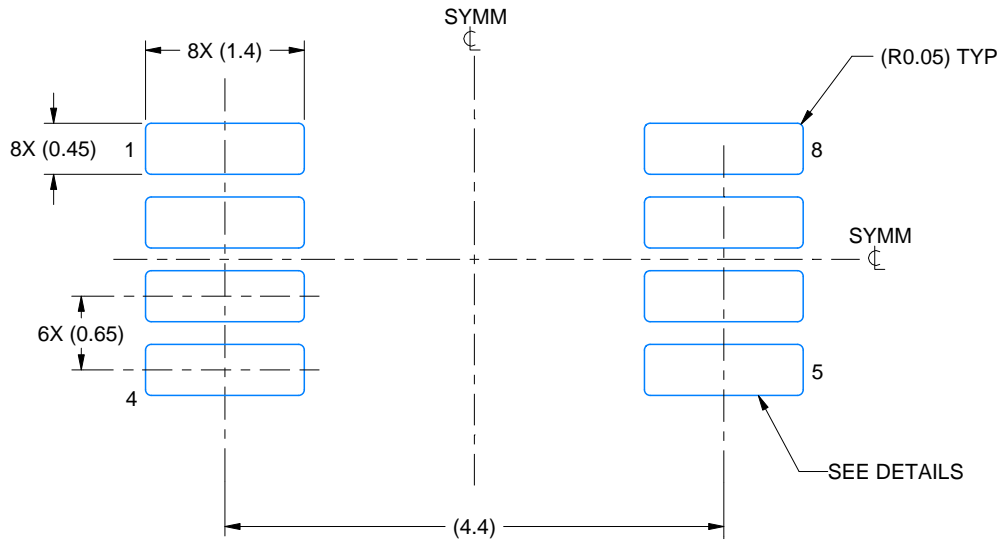
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-187.

EXAMPLE BOARD LAYOUT

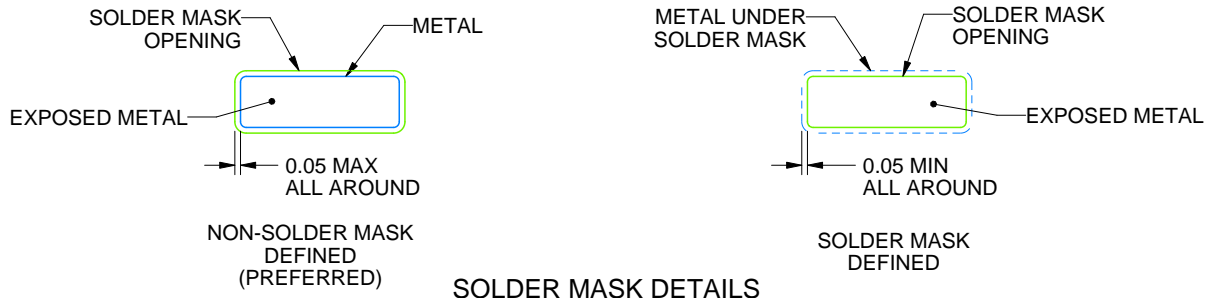
DGK0008A

TM VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE: 15X



SOLDER MASK DETAILS

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NOTES: (continued)

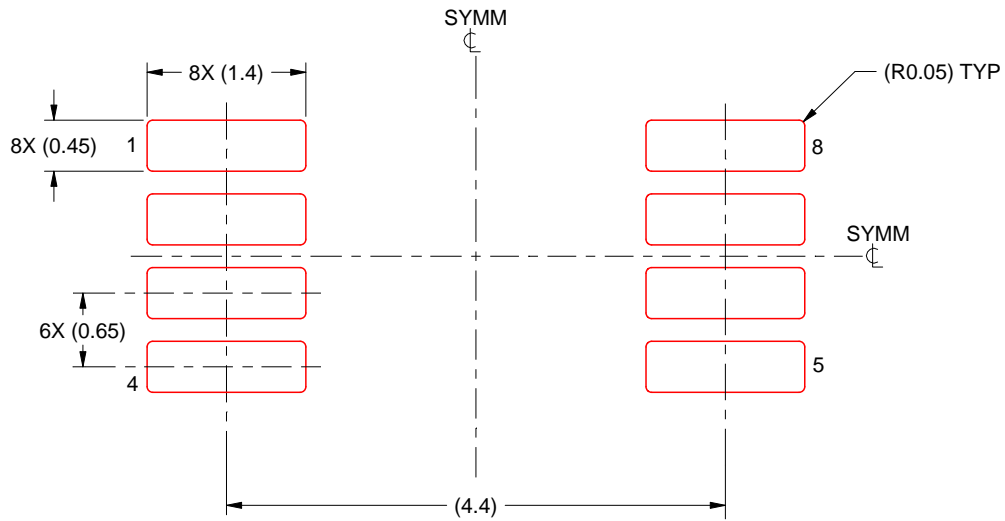
6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.

EXAMPLE STENCIL DESIGN

DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE
SCALE: 15X

4214862/A 04/2023

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

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